

TRIGGERED SWEEP OSCILLOSCOPE

HIGH STABILITY

CS-1560AI

DUAL TRACE OSCILLOSCOPE

INSTRUCTION MANUAL



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FEATURES

- * Vertical axis of low input capacitance ($22 \pm 3\text{pF}$) for 2-channel operation provides high sensitivity and wide band-width (10mV/div , 15MHz).
- * High sensitivity CRT with excellent beam permeability has sufficient brightness for measurements of fast speed pulses of high frequencies.
- * The high voltage power for CRT as well as the power for other circuits is fully stabilized because of the use of DC-DC converter, thus the sensitivity and brightness are completely free from effects of voltage variations.
- * X-Y operation is possible with CH2 amplifier used as X axis.
The horizontal axis sensitivity is as high as 10mV/div , permitting accurate calibrations.
- * Time base switch allows changeover between CHOP and ALT and between V(vertical) and H(horizontal) of TV sync

- separator circuit, automatically and electronically.
- * CH1 and CH2 can be individually synchronized (internal synchronization).
- * At AUTO position of TRIG LEVEL, it is possible to check the brightness at no-signal time and to adjust triggering level of input waveforms.
- * Mode selector switch is provided for measurements of sum and difference between 2 channels.
- * Low power consumption (23W) for cool operation.
- * All component parts are cleverly mounted on circuit boards for improved reliability.
- * Trace rotation system for easy adjustment of horizontal trace.
- * The adoption of IC's throughout circuitry assures high performance and improved reliability.

SPECIFICATIONS

Cathode Ray Tube

Type: 130BXB31 or C535P31B
 Accelerating voltage: 2kV
 Scale: 8 div \times 10 div (1 div = 1 cm)

Vertical Amplifiers (CH1 and CH2)

Deflection Factor: 10 mV/div \sim 20V/div,
 1-2-5 sequence (1 div = 1 cm)
 Precisely adjustable between all ranges.
 Sensitivity error between ranges is $\pm 5\%$.

Input Impedance: $1\text{M}\Omega \pm 5\%$
 Input Capacitance: $22\text{pF} \pm 3\text{pF}$
 Frequency Response: DC DC - 15MHz (less than -3dB)
 AC 2Hz - 15MHz (less than -3dB)

Rising Time: Less than 23 nsec.
 Over-shoot: Less than 3%
 (at 100kHz square wave)

Cross-talk: Better than 70dB at 1kHz
 Operating Modes:
 CH1 Channel 1 only
 CH2 Channel 2 only
 DUAL Dual trace (CHOP and ALT are automatically selected by SWEEP TIME/DIV) $0.5\mu\text{s/div} \sim 0.5\text{ms/div}$
 ALT (alternate sweep) $1\text{ms/div} \sim 0.5\text{s/div}$.
 CHOP (200 kHz switching)
 ADD Algebraic sum of CH1 and CH2.
 SUB Algebraic difference of CH1 and CH2.

CHOP Frequency: 200kHz $\pm 20\%$

Maximum Input

Voltage: 600Vp-p or 300V (DC + AC peak)

Sweep Circuit (Common to CH1 and CH2)

Sweep System: Triggered and automatic. In automatic mode, sweep is obtained without input signal.

Sweep Time: $0.5\mu\text{s/div} \sim 0.5\text{s/div} \pm 5\%$ and "X-Y", 1-2-5 sequence Fine adjustment between all 19 ranges

Sweep Magnification: Obtained by enlarging the above sweep 5 times ($\pm 5\%$) from center.

Linearity: Less than 3% ($2\mu\text{s/div} \sim 0.5\text{s/div}$)
 Less than 5% ($0.5\mu\text{s/div} \sim 1\mu\text{s/div}$)

Triggering

Source: CH1, CH2 and EXT
 Slope: NORM - positive and negative
 TV- positive and negative
 (TVH and TVV are automatically switched by SWEEP TIME/DIV)
 TVH (TV - Line): $0.5\mu\text{s/div} \sim 50\mu\text{s/div}$
 TVV (TV - Field): $0.1\text{ms/div} \sim 0.5\text{s/div}$

Triggering Voltage: CH1 and CH2..... Amplitude on CRT screen, more than 0.5div
 EXT..... More than 1Vp-p

Triggering Range: 20Hz \sim 15MHz

Horizontal Amplifier (Horizontal input thru CH2 input)

X-Y Operation: With SWEEP TIME/DIV switch in X-Y position, the CH1 input becomes the Y input (vertical) and the CH2 input becomes the X input (horizontal). The CH2 position control becomes the horizontal position control.

Deflection Factor: Same as CH2 (10mV/div ~ 20V/div $\pm 5\%$)

Frequency Response: DC DC - 1MHz (less than -3dB)
AC2 Hz - 1MHz (less than -3dB)

Input Impedance: Same as CH2 (1M Ω $\pm 5\%$)

Input Capacitance: Same as CH2 (22pF $\pm 3\text{pF}$)

Calibrating Voltage: 1VP-p $\pm 5\%$
(1kHz square wave)

Intensity Modulation

Input Voltage: More than 20Vp-p

Input Impedance: 470k Ω $\pm 20\%$

Trace Rotation: More than 20Vp-p

Input Impedance: 470k Ω $\pm 20\%$

Trace Rotation: Trace angle is adjustable by panel surface adjustor.

Power Requirements

Power Supply Voltage: AC 100/117/220/240V $\pm 10\%$,
50/60Hz

Power Consumption: 23W

Dimensions and Weight

Width: 260mm (277mm)

Height: 190mm (204mm)

Depth: 384mm (449mm)

Figures in () show maximum sizes.

Weight: 9.3 kg

Accessory

Probe: PC-27 2
Damping 1/10
Input impedance 10M Ω
Input capacitance less than 18pF

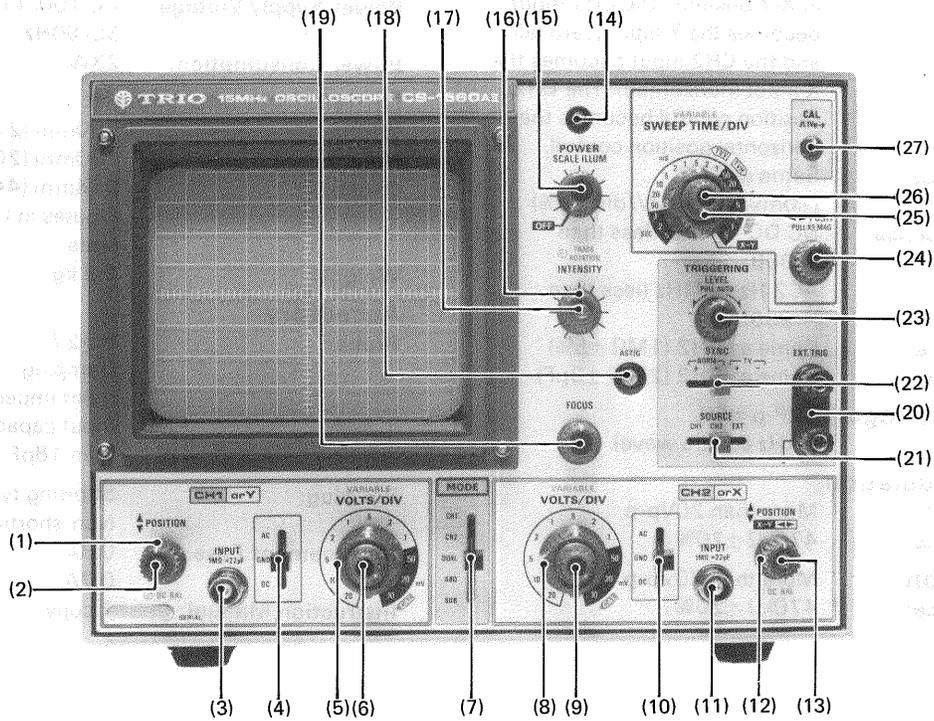
Pin-plug: Shorting type 1
Non-shorting type 1

Replacement Fuse: 0.3A 2
0.7A 2

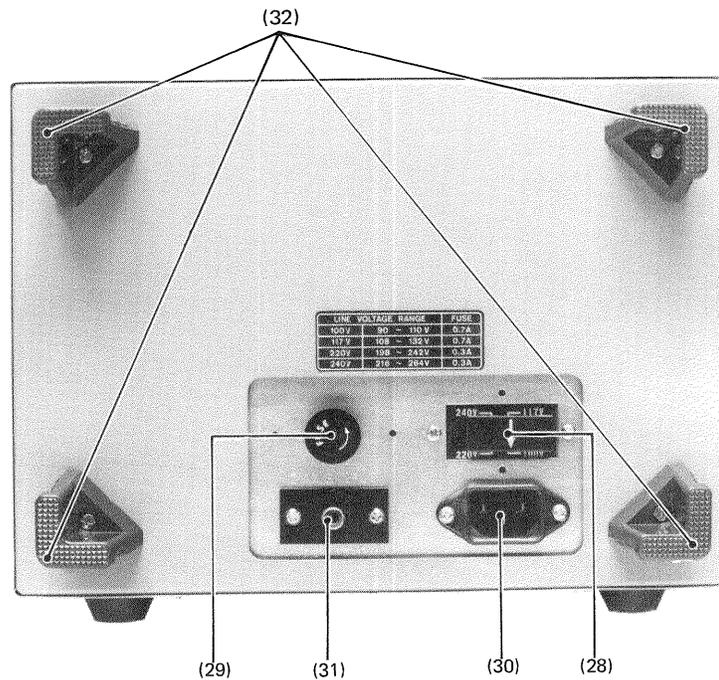
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CONTROLS ON PANELS

FRONT PANEL



REAR PANEL



1. \blacktriangle POSITION

This control adjusts vertical position during CH1 operation and Y position during X-Y operation. Waveforms can be set to any desired vertical position. A right turn of the control will shift waveform upward, and vice versa.

2. DC BAL

Vertical DC balance adjustment for CH1(or Y). Adjustment is made so that waveform position is not shifted when the gain control VARIABLE(6) for the vertical amplifier is rotated.

3. INPUT

Vertical input terminal for CH1, or Y input terminal during X-Y operation.

4. AC-GND-DC

Vertical input selector for CH1, or for Y input selector during X-Y operation.

AC: The DC component of input signal is blocked by capacitor.

GND: The input terminal opens and the input of internal amplifier is grounded.

DC: The input terminal is directly connected to the amplifier and all components of input signal are amplified.

5. VOLTS/DIV

Vertical attenuator for CH1 or for Y during X-Y operation. The scale is graduated in voltage per "div" (= cm) of CRT screen area. Calibrated voltage is indicated when VARIABLE (6) is turned fully clockwise. Set this control for proper waveform according to the input voltage used. Selectable in 11 ranges from 10mV/div to 20V/div.

6. VARIABLE

Vertical attenuator for the control of vertical sensitivity of CH1 or Y during X-Y operation. It continuously controls between 11 ranges of VOLT/DIV (5). In the extreme clockwise (CAL) position, the vertical attenuator is calibrated.

7. MODE(CH1, CH2, DUAL, ADD, SUB)

CH1: Only the input signal to CH1 is displayed as a single trace.

CH2: Only the input signal to CH2 is displayed as a single trace.

DUAL: In the range of 0.5s/div to 1ms/div, the input signals to both channels are switched by about 200 kHz signal (CHOP operation).

In the range of 0.5ms/div to 0.5 μ s/div, the input signals to both channels are alternately switched for each sweep (ALT operation).

ADD: The waveforms from both channel inputs are algebraically added and the sum is displayed as a single trace.

SUB: The input of reverse polarity to CH2 is added to the input to CH1 and the algebraic difference obtained between CH1 and CH2 is displayed as a single trace.

If CH1 has no input or it is grounded, the waveform of reverse polarity from CH2 input is displayed.

8. VOLTS/DIV

Vertical attenuator for CH2. It has the same function as VOLT/DIV(5), but is also used as X attenuator during X-Y operation.

9. VARIABLE

Vertical attenuator adjustment provides fine control of vertical sensitivity of CH2. It has the same function as VARIABLE(6), but is also used as X fine adjuster.

10. AC-GND-DC

Vertical input selector for CH2. It has the same function as AC-GND-DC(4), but is also used as X input selector.

11. INPUT

Vertical input terminal for CH2 or X input terminal during X-Y operation.

12. \blacktriangle POSITION, X-Y \blacktriangle

Vertical position adjuster for CH2. It functions the same as \blacktriangle POSITION(1), but is also used as X position adjuster during X-Y operation.

13. DC BAL

Vertical DC balance adjustment for CH2(or X). It has the same function as DC BAL(2).

14. LED Pilot Lamp

This lamp lights as the power switch ILLUM(15) is turned on.

15. POWER/SCALE ILLUM

Power is turned off at the extreme left turn position. A right turn will set the power to ON and illuminate the dial scale.

16. INTENSITY

Adjusts the brightness of spots and waveforms for easy viewing. A left turn will allow the waveform to disappear.

17. TRACE ROTATION

This is used to eliminate inclination of horizontal trace.

18. ASTIG

Astigmatism adjustment provides optimum spot roundness and brightness when used with FOCUS(19). Once it is adjusted, no further adjustments are required.

19. FOCUS

Spot focus control to obtain optimum waveform according to brightness.

20. EXT TRIG

External triggering terminal. For external triggering, external triggering voltage (more than 1Vp-p) should be applied, with SOURCE switch (21) set to EXT.

21. SOURCE

Three-position switch to select triggering voltages for CH1, CH2 and EXT.

CH1: Sweep is triggered by CH1 vertical input waveform.

Both sweeps are triggered by the same source in dual(2-channel) trace operation.

CH2: Sweep is triggered by CH2 vertical input waveform.

Both sweeps are triggered by the same source in dual (2-channel) trace operation.

EXT: Sweep is triggered by an external signal applied to EXT TRIG (20) terminal.

22. SYNC

Sync separator switch. It picks up sync signal component in TV video signal and applied to trigger circuit for complete synchronization of video signal being viewed.

NORM ±: Used for viewing general waveforms. In this position, TV sync separator circuit is not connected.

At “+” polarity, sweep is effected by “+” slope and, at “-” polarity, by “-” slope.

TV ±: Used for viewing waveforms with TV video signal synchronized with sync signal. TVV and TVH are automatically selected for sweep times of 0.5s to 0.1ms and 50 μ s to 0.5 μ s of SWEEP TIME/DIV rotary switch, respectively, and are synchronized with vertical and horizontal sync signals.

Polarity should be set to match that of video signal as shown in the illustration.

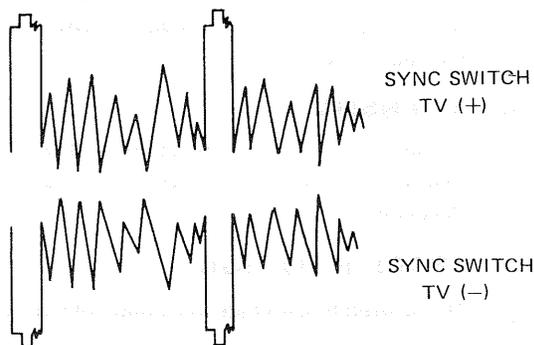


Fig. 1

23. LEVEL

Triggering level control adjusts sync phase to determine the starting point of sweep on the slope of trigger signal waveform.

PULL AUTO:

By pulling LEVEL VR toward you, auto-sweep is effected; the sweep is set in free-running state even when no trigger input signal is applied, with fly-back line displayed on CRT.

With trigger signal, trigger-sweep is effected where sync level is adjustable. When the sync level exceeds the limit, the sweep is set in free-running state.

24. ◀▶ POSITION, PULL X5 MAG

Horizontal position adjuster to shift waveform to any desired horizontal position. A right turn of the adjuster will shift the waveform to right, and vice versa.

pull × 5 MAG.

Sweep magnifier switch. By pulling the knob toward you, waveform is magnified to 5 times in left and right directions. Brightness is slightly decreased.

25. SWEEP TIME/DIV

Horizontal sweep time selector. It selects sweep times of 0.5 μ s to 0.5s in 19 steps. X-Y operation is possible by turning the knob fully clockwise. Changeover between CHOP, ALT, TVV and TVH is also accomplished automatically by this selector. When VARIABLE (26) is turned fully clockwise, calibrated reading is obtained which is the sweep time per “div”.

26. VARIABLE

Used for fine adjustment of sweep time. Continuous adjustment between 19 steps of SWEEP TIME/DIV (25) is possible. Sweep time is calibrated at the extreme clockwise position (CAL).

27. CAL

Calibration voltage terminal. Calibration voltage is 1Vp-p of about 1kHz square wave.

28. AC VOLTAGE SELECTOR

The CS-1560A II may be operated from 100V, 120V, 220V, 240V, putting the AC VOLTAGE SELECTOR in the place of another.

29. FUSE HOLDER

For 100 ~ 120V operation a 0.7 ampere fuse should be used.

For 220 ~ 240V operation a 0.3 ampere fuse should be used.

30. POWER CONNECTOR

For connection of the supplied AC power cord.

31. Z AXIS INPUT

Intensity (brightness) modulation terminal. Intensity is modulated at voltages of 20Vp-p or higher. When modulation is not needed, the supplied shorting pin must be plugged in.

32. CORD REEL

Wind power cord when the oscilloscope is to be carried or stored. They also serve as a stand when the oscilloscope is used in upright position.

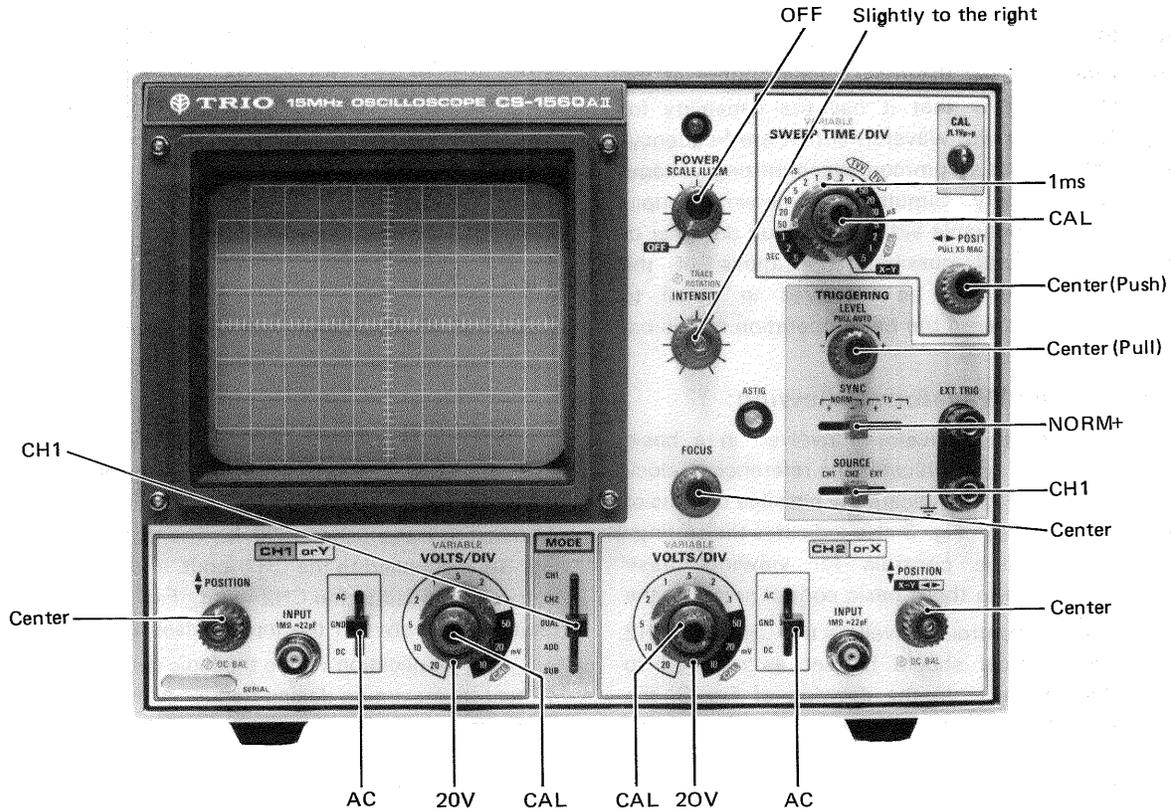
OPERATION

PRELIMINARY OPERATION

When operating this oscilloscope, refer to panel controls and

their functions (see page 4).

When starting this oscilloscope set initially, set the operating controls as follows and the set may be turned on safely.



OPERATING PROCEDURES

- (1) Insert the supplied power cord to the power connector. Then, select the position of the power voltage selector plug as indicated by the arrow marks.
- (2) Turn POWER (15) clockwise. The power is turned to ON and LED pilot lamp (14) lights.
- (3) Horizontal axis will be displayed. When fly-back line does not appear at the center of the screen, adjust POSITION (1) and POSITION PULL $\times 5$ MAG (24). Adjust brightness with INTENSITY (16). If fly-back line is unclear, adjust FOCUS (19).
- (4) The oscilloscope is now ready for measurement. For measurement, proceed as follows:
Apply signal voltages to the Input terminals (3), (11). Then turn VOLT/DIV (5) clockwise until the waveform is correctly displayed on the scope. By setting MODE (7) and SOURCE (21) to CH1, the CH1 input signal to the Input terminal (3) will appear. Similarly, by setting MODE and SOURCE to CH2, then the input signal to the CH2 terminal (11) will appear. When MODE (7) is set to DUAL, two waveforms (CH1 and CH2) will appear on the scope. With SOURCE (21) set to CH1, the CH1 input signal from the Input terminal (3) is fed to

the synchro circuit where the CH1 signal is synchronized. Similarly, when SOURCE is set to CH2, the CH2 signal is synchronized. Use either method for easier observation.

When MODE is set to ADD, the CH1 signal is algebraically added to the CH2 signal; and when it is set to SUB, the CH2 signal in reverse polarity is added to the CH1 signal and the algebraic difference between CH1 and CH2 is displayed.

- (5) When the signal voltage is more than 10 mV and waveform fails to appear on the screen, the oscilloscope may be checked by feeding input from CAL 1Vp-p (27). Since calibration voltage is 1Vp-p, the waveform becomes 5div high at the 0.2V/div position.
- (6) By pushing LEVEL (23), the free-running auto function is released. The waveform disappears when the knob is turned clockwise, and appears again at the approximate mid position of it. Sync phase is also adjustable in this case. The waveform will again disappear when the knob is turned counterclockwise from the mid position.
- (7) When DC component is measured, set AC-GND-DC to DC position. If, in this case, the DC component con-

tains plus "+" potential, the waveform moves upward and if it contains minus "-" potential, the waveform moves downward.

The reference point of "0" potential is checked at GND position.

APPLICATIONS

DUAL-TRACE APPLICATIONS

Introduction:

The most obvious and yet the most useful feature of the dual-trace oscilloscope is that it has the capability for simultaneously viewing two waveforms that are frequency- or phase-related, or that a common synchronizing voltage, such as in digital circuitry. Simultaneous viewing of input and its output is an invaluable aid to the circuit designer or the repairman. Several possible applications of the dual-trace oscilloscope will be reviewed in detail to familiarize the user further in the basic operation of this oscilloscope.

Frequency Divider Waveforms Viewing:

Fig. 3 illustrates the waveform involved in a basic divide-by-two circuit. Fig. A indicates the reference or clock pulse train. Fig. B and Fig. C indicate the possible outputs of the divide-by-two circuitry. Fig. 3 also indicates the settings of specific oscilloscope controls for viewing these waveforms. In addition to these basic control settings, the TRIGGERING LEVEL control, as well as the CH1 and CH2 vertical position controls should be set as required to produce suitable displays. In the drawing of Fig. 3, the waveform levels of 2 cm are indicated. If exact voltage measurements of CH1 and CH2 are desired, the CH1 and CH2 VARIABLE controls must be placed in the CAL position. The CH2 waveform may be either that indicated in Fig. 3B or Fig. 3C. In Fig. 3C, the divide-by-two output waveform is shown which occurs during the falling time of pulses. In this case, the putput waveform is shifted with

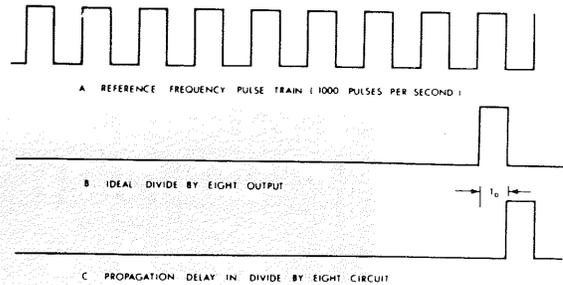


Fig. 2. Waveforms in divide-by-eight circuit

respect to the leading edge of the reference frequency pulse by a time interval corresponding to the pulse width.

Divide-by-8 Circuit Waveforms:

Fig. 2 indicates waveform relationships for a basic divide-by-eight circuit. The oscilloscope settings are identical to those used in Fig. 4. The reference frequency of Fig. 3A is supplied to the CH1 input, and the divide-by-eight output is applied to the CH2 input. Fig. 2 indicates the time relationship between the input pulses and output pulses.

In an application where the logic circuitry is operating at or near its maximum design frequency, the accumulated rise time effects of the consecutive stages produce a built-in time propagation delay which must be compensated for. Fig. 2C indicates the possible time delay which may be introduced into a frequency divider circuit. Use of the dualtrace oscilloscope, the input and output waveforms can be superimposed (ADD or SUB) to measure the exact amount of propagation delay that occurs.

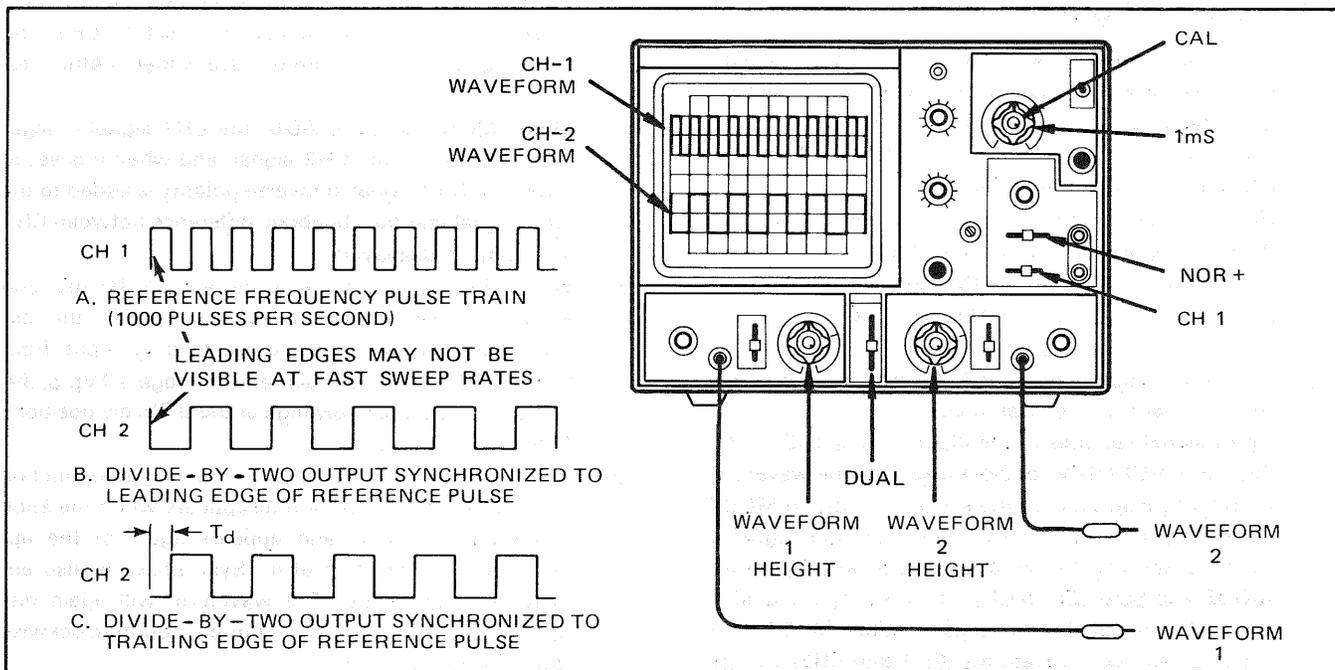


Fig. 3. Waveforms in divide-by-two circuit

Propagation Delay Time Measurement:

An example of propagation delay in a divide-by-eight circuit was given in the previous paragraph. Significant propagation delay may occur in any circuit. This oscilloscope has features which simplify measurement of propagation delay. Fig. 5 shows the resultant waveforms when the dual-trace presentation is combined into a single-trace presentation by selecting the ADD or SUB position of the MODE switch. In the ADD position the two inputs are

algebraically added in a single-trace display. Similarly, in the SUB position the two inputs are algebraically subtracted. Either position provides a precise display of the propagation time (T_p). Using the calibrated time base (CAL), T_p can be measured. A more precise measurement can be obtained if the T_p portion of the waveform is expanded horizontally by pulling the 5X MAG control. It also may be possible to view the desired portion of the waveform at a faster sweep speed.

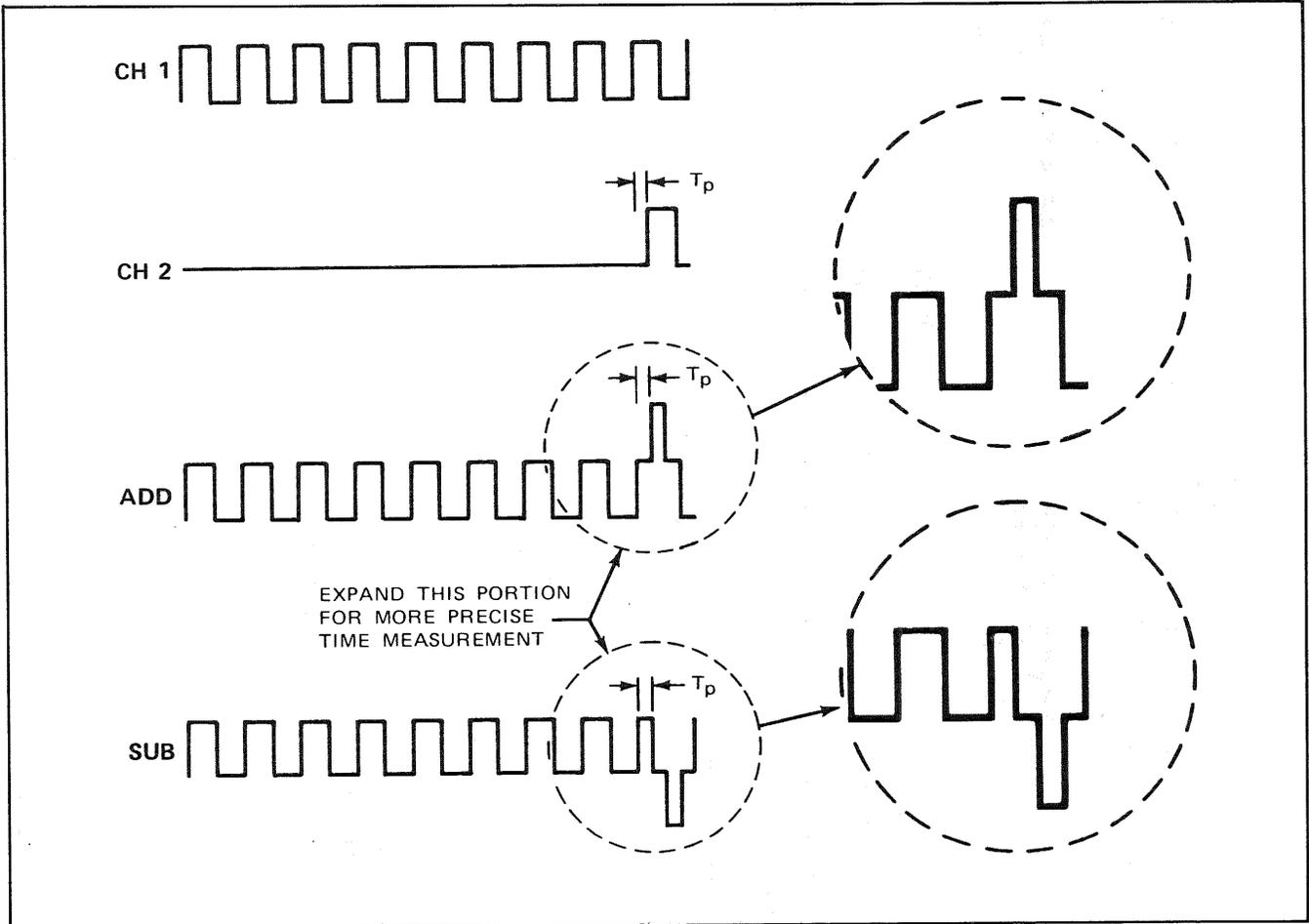


Fig. 4. Using ADD or SUB modes for propagation time measurement

Digital Circuit Time Delay Measurement:

Since a dual-trace oscilloscope has the capability of comparing the timing of one waveform with another, it is necessary in designing, manufacturing and servicing digital equipment. In digital equipment, many of the circuits are frequency dividers as previously described, but waveforms are often time-related in many other combinations. Fig. 5 shows a typical digital circuit and identifies several of the points at which waveform measurements are appropriate. Under the operating condition, waveforms will vary according to the input or operating mode. Fig. 6 shows the relationship between the normal waveforms to be expected at each of these points and their timing. If the correct time relationship with respect to other waveform is unknown, measurement of individual waveforms means nothing. The dual-trace oscilloscope allows this comparison to be made. In an application, waveform No. 3 would be displayed on

CH1 and waveform No. 4 thru No. 8 and No. 10 would be displayed on CH2. Waveforms No. 11 through No. 13 would probably be displayed on CH2 in relationship to waveform No. 8 or No. 4 on CH1. No. 8 or No. 10 is an excellent sync source for viewing all of the waveforms.

With No. 8 or No. 10 used as external sync source, any of the waveforms may be displayed without readjustment of the TRIG LEVEL control. Waveforms No. 4 through No. 7 should not be used as the sync source because they do not contain a triggering pulse at the start of the frame. It would not be necessary to view the entire waveforms as shown in Fig. 6 in all cases. In fact, there are many times when a closer examination of a portion of the waveforms would be appropriate. In such cases, it is recommended that the sync remain unchanged while the sweep speed be increased or X5 MAG control used to expand the waveform display.

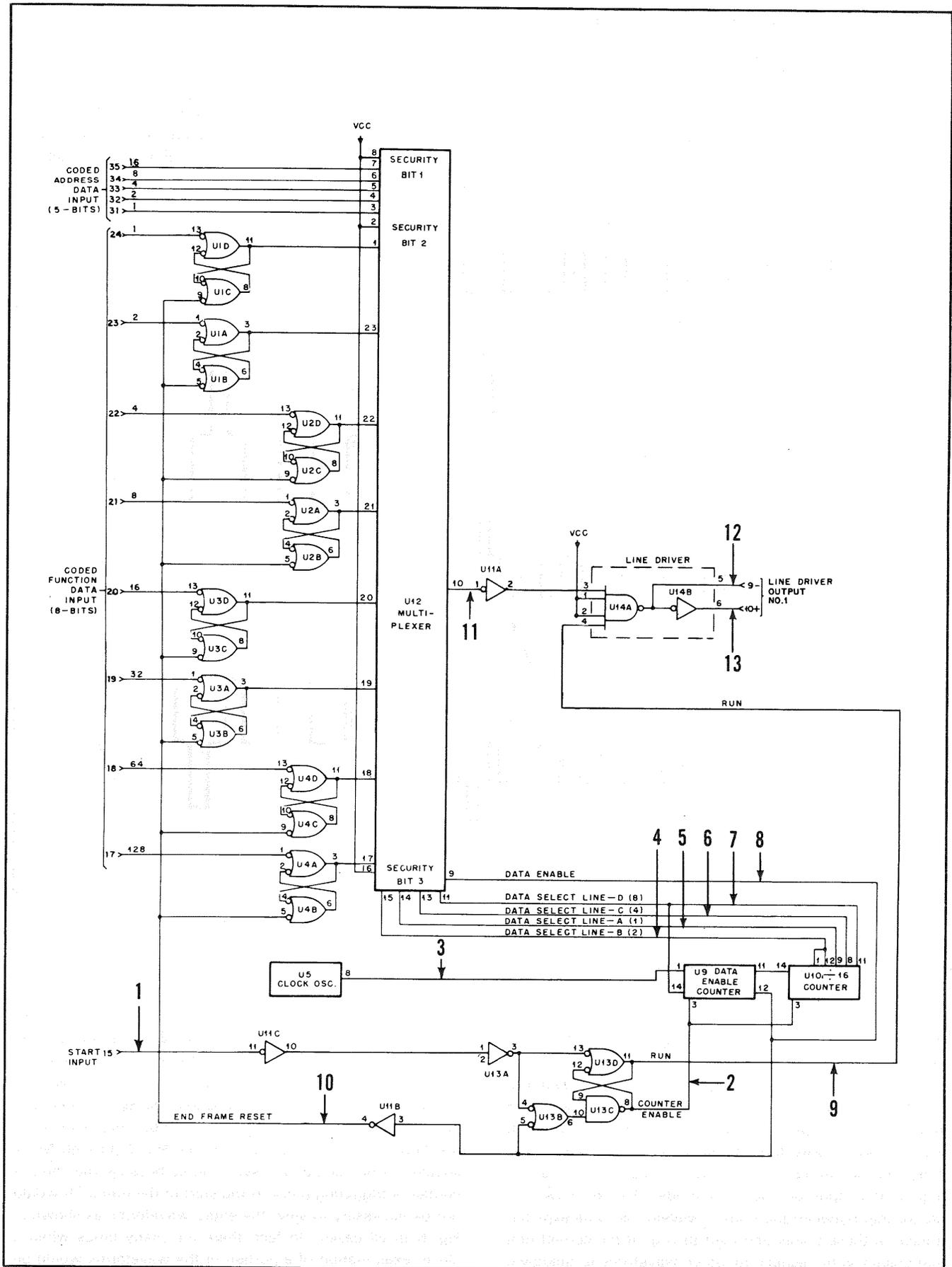


Fig. 5. Typical digital circuit using several time-related waveforms

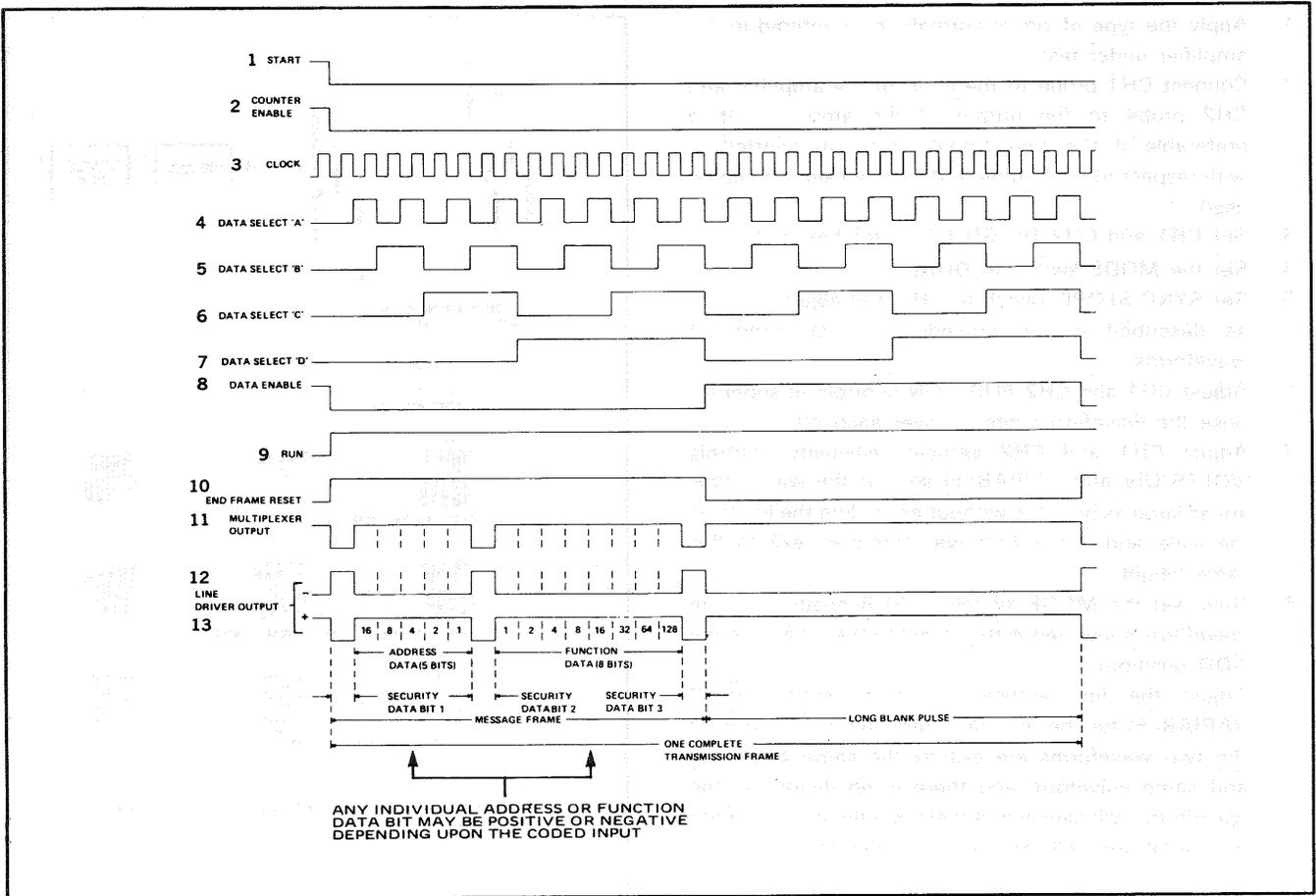


Fig. 6. Family of time-related waveforms from typical digital circuit in Fig. 5

Distortion Measurement:

Distortion of an amplifier may be measured with this oscilloscope. This measurement is especially variable when the slope of a waveform must be faithfully reproduced by an amplifier. Fig. 7 shows the testing of a circuit using a triangular wave, such as is found in the limiter circuit of a

transmitter modulator. The measurement may be made using any type of signal; merely use the type of signal for testing that is normally applied to the amplifier during normal operation. The procedure for distortion testing is as follows:

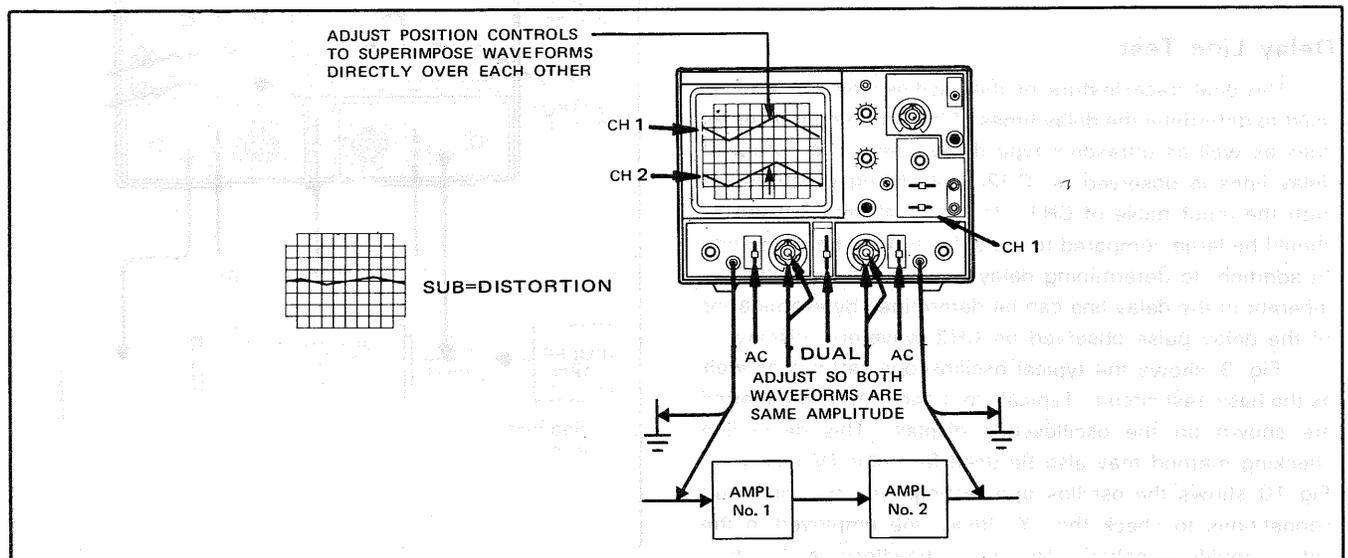


Fig. 7. Distortion measurement

1. Apply the type of signal normally encountered in the amplifier under test.
2. Connect CH1 probe to the input of the amplifier and CH2 probe to the output of the amplifier. It is preferable if the two signals are not inverted with respect to each other, but inverted signals can be used.
3. Set CH1 and CH2 DC-GND-AC switches to AC.
4. Set the MODE switch to DUAL.
5. Set SYNC SLOPE switch to CH1 and adjust controls as described in the procedure for synchronizing waveforms.
6. Adjust CH1 and CH2 POSITION controls to superimpose the waveforms directly over each other.
7. Adjust CH1 and CH2 vertical sensitivity controls (VOLTS/DIV and VARIABLE) so that the waveforms are as large as possible without exceeding the limits of the scale, and so that both waveforms are exactly the same height.
8. Now, set the MODE switch to SUB position (if one waveform is inverted with respect to the other, use the ADD position).
Adjust the fine vertical sensitivity control (CH2 VARIABLE) for the minimum remaining waveform; if the two waveforms are exactly the same amplitude and same waveform and there is no distortion, the waveforms will cancel and there will be only a straight horizontal line will remain on the screen.

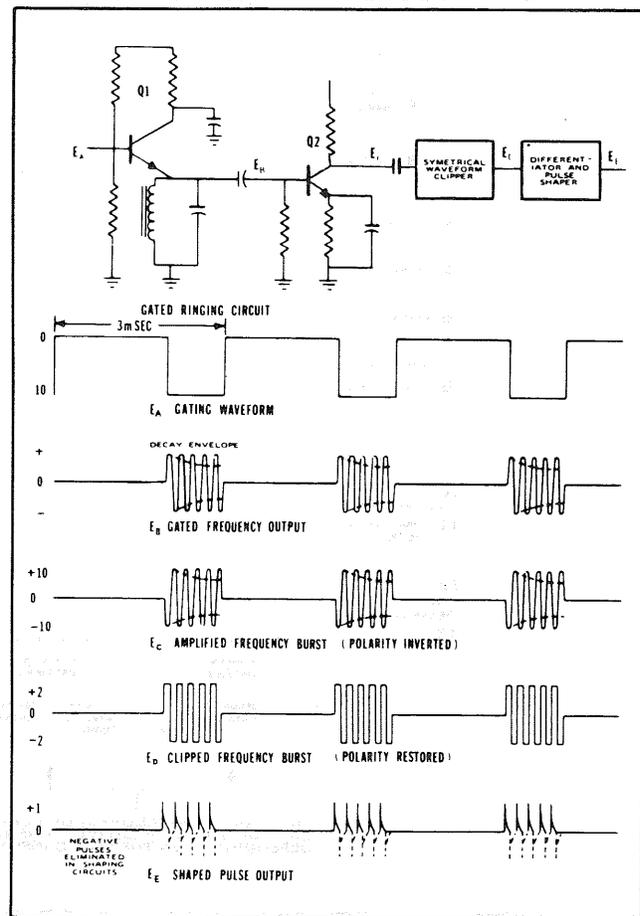


Fig. 8. Gated ringing circuit and waveforms

Gated Ringing Circuit(burst circuit):

Fig. 8 shows a burst circuit. The basic settings of control knobs are the same as those in Fig. 4. The waveform A is the reference waveform and is applied to CH1 input. All other waveforms are sampled at CH2 and compared to the reference waveform of CH1. The burst signal can be examined more closely either by increasing the sweep time or by pulling the ◀▶ POSITION control to obtain 5 times magnification.

Delay Line Test:

The dual-trace feature of the oscilloscope can also be used to determine the delay times of transmission type delay lines as well as ultrasonic type delay lines. The output of delay lines is observed on CH2 while being synchronized with the input pulse of CH1. The interval between pulses should be large compared to the delay time to be observed. In addition, to determining delay time, the pulse distortion inherent in the delay line can be determined by examination of the delay pulse observed on CH2 waveform display.

Fig. 9 shows the typical oscilloscope settings as well as the basic test circuit. Typical input and output waveforms are shown on the oscilloscope display. This delay line checking method may also be used for color TV receivers. Fig. 10 shows the oscilloscope settings and typical circuit connections to check the "Y" delay line employed in the video amplifier section. The input waveform and output

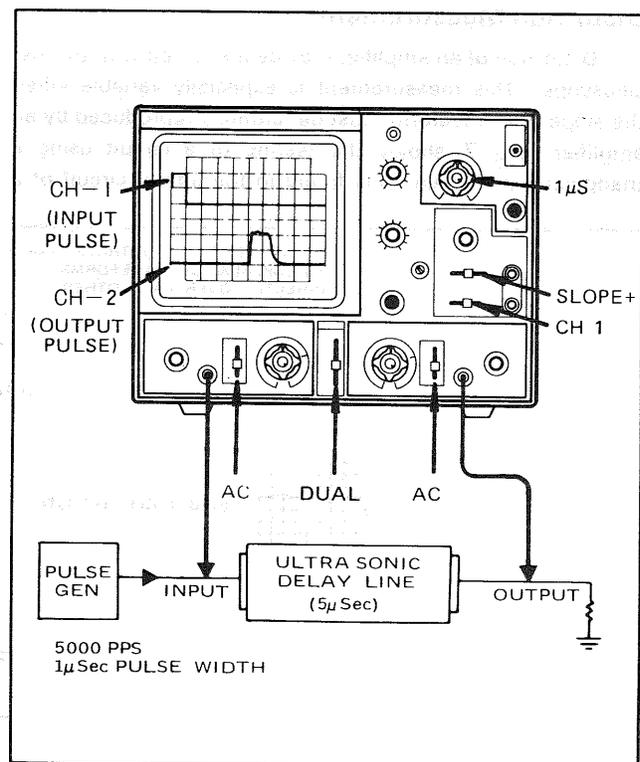


Fig. 9. Delay line measurements

waveform are compared for delay time, using the horizontal sync pulse of the composite video signal for reference. The indicated delay is approximately one microsecond. In addition

to determining the delay characteristics of the line, the output waveform reveals any distortion that may be introduced from an impedance mismatch.

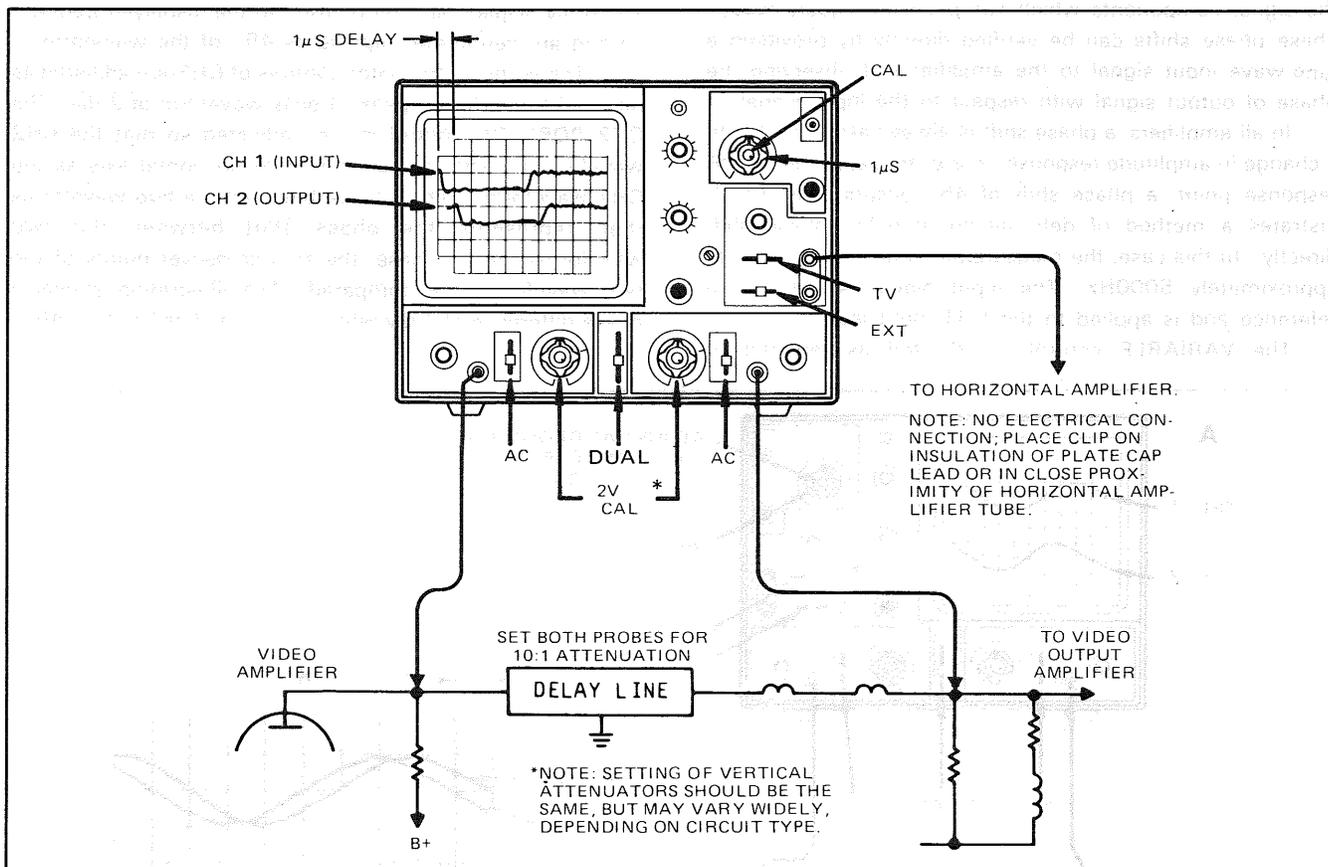


Fig. 10. Checking "Y" delay line in color television receivers

Stereo Amplifier Servicing:

Another convenient use for a dual-trace oscilloscope is in troubleshooting stereo amplifiers. If identical amplifiers are used and the output of one is weak, distorted or otherwise abnormal, the dual-trace oscilloscope can be efficiently used to localize the defect. With an identical signal applied to the inputs of both amplifiers, a side-by-side comparison of both units can be made by progressively sampling identical signal points in both amplifiers. When the defective or malfunctioning stage has been located, it can be immediately observed and analyzed.

Improving the Ratio of Desired to Undesired Signals:

In some applications, the desired signal may be riding on a large undesired signal component such as 60 Hz. It is possible to minimize or for practical purpose eliminate the undesired component. Fig. 11 shows the oscilloscope settings for such an application. The waveform display of CH1 indicates the desired signal and the dotted line indicates the average amplitude variation corresponding to the undesired 60 Hz component. The CH2 display indicates a waveform of equal amplitude and identical phase to the average of the CH1 waveform. With the MODE switch set to SUB, and by adjusting the CH2 vertical attenuator con-

trol, the 60 Hz component of the CH1 signal can be cancelled by the CH2 input and the desired waveform can be observed.

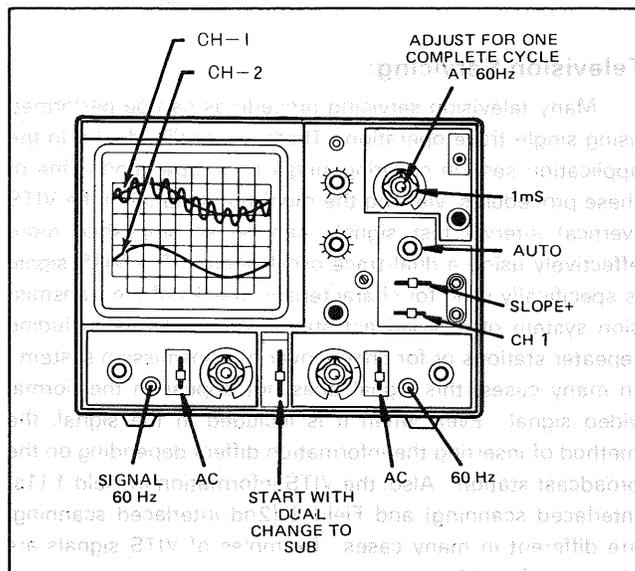


Fig. 11. Improving desired-to-undesired signal ratio

Amplifier Phase Shift Measurements:

In the square wave testing section of this manual, square wave distortion is explained in terms of phase shift of the signal components which comprise the square wave. These phase shifts can be verified directly by providing a sine wave input signal to the amplifier and observing the phase of output signal with respect to the input signal.

In all amplifiers, a phase shift is always associated with a change in amplitude response. For example, at the -3dB response point, a phase shift of 45° occurs. Fig. 11 illustrates a method of determining amplifier phase shift directly. In this case, the measurements are being made at approximately 5000Hz . The input signal is used as a reference and is applied to the CH1 input jack.

The VARIABLE control is adjusted as required to

provide a complete cycle of the input waveform displayed on 8 div horizontally, while the waveform height is set to 2 div. The 8 div display represents 360° at the displayed frequency and are centimeter represents 45° of the waveform.

The vertical attenuator controls of CH2 are adjusted as required to produce a peak-to-peak waveform of 2 div. The CH2 POSITION control is then adjusted so that the CH2 waveform is displayed on the same horizontal axis as the CH1 waveform. The distance between the two waveforms then represents the phase shift between the two waveforms. In this case, the zero crossover points of the two waveforms are compared. The illustration shows a phase difference of 1 div which means a phase shift of 45° .

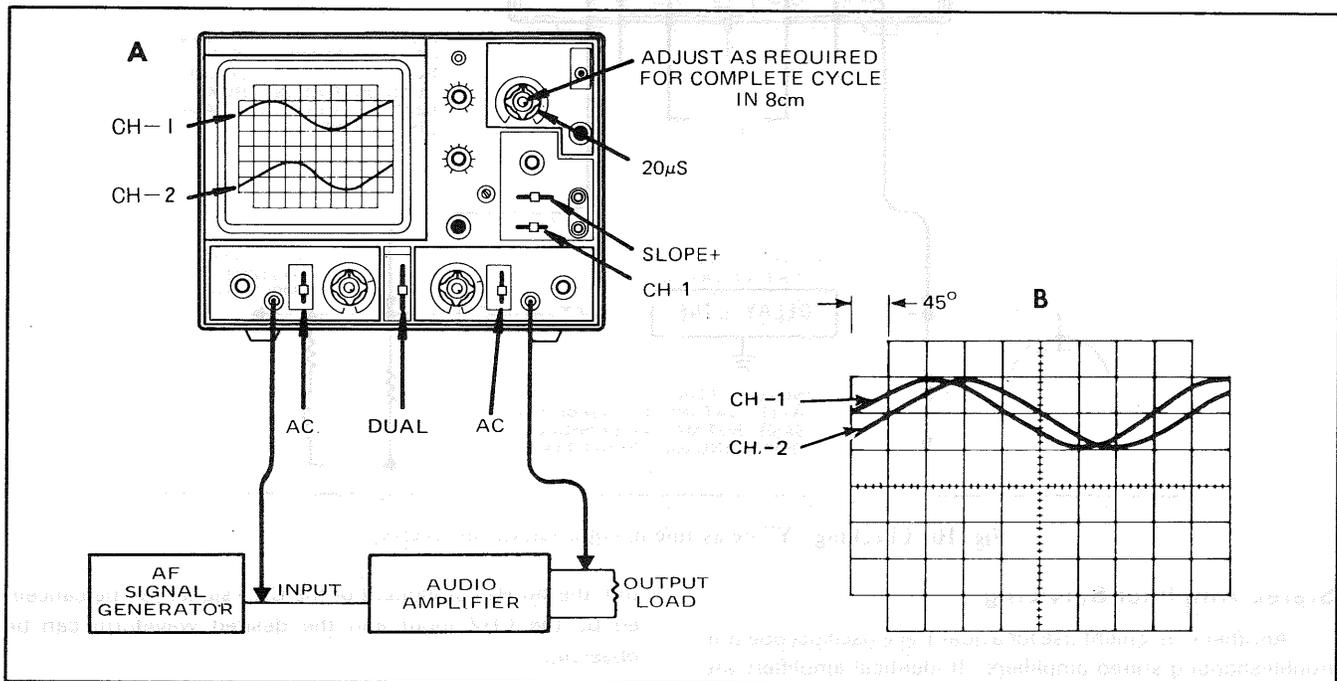


Fig. 12. Measuring amplifier phase shift

Television Servicing:

Many television servicing procedures can be performed using single-trace operation. These are outlined later in the application section covering single-trace operation. One of these procedures, viewing the multi-burst signal in the VITS (vertical interval test signal), can be accomplished more effectively using a dual-trace oscilloscope. The VITS signal is specifically used for characteristic checks of the transmission system of a broadcast station or a network including repeater stations or for changeover of transmission system. In many cases, this signal does not appear in the normal video signal. Even when it is included in the signal, the method of inserting the information differs depending on the broadcast station. Also, the VITS information in Field 1 (1st interlaced scanning) and Field 2 (2nd interlaced scanning) are different in many cases. Examples of VITS signals are shown in Fig. 13.

Because the oscilloscope sweep is synchronized to the vertical blanking signal, the waveform of Field 1 cannot be

distinguished from that of Field 2. This causes the VITS signals to be superimposed onto each other, resulting in difficulty in viewing. With dual-trace operation using the same input, the waveform can be viewed separately without overlapping because of the effects of the oscilloscope's alternate sweep operation and interlaced scanning of TV signal.

The possibility of viewing VITS signal provides an important role in servicing TV sets. This VITS signals can localize trouble in the antenna, tuner, IF or video sections and shows when realignment may be required. The following procedures show how to analyze and interpret oscilloscope displays of the VITS.

The VITS is transmitted during the vertical blanking interval. On the television set, it can be seen as a bright white line above the top of the picture, when the vertical linearity or height is adjusted to view the vertical blanking interval (on TV sets with internal retrace blanking circuits, the blanking circuits must be disabled to see the VITS).

The transmitted VITS has a specific frequency, amplitude and waveform as shown in Fig. 14. Television networks use precise signals for adjustment and checking of network transmission equipment, but the multi-burst signal in VITS can also be used for checking the operating

condition of TV sets. The first frame of VITS at the "B" section (line 18) in Fig. 14 begins with a white reference signal, followed by sine wave frequencies of 0.5MHz, 1.0MHz, 2MHz, 3MHz, 4.0MHz and 3.58MHz. This sequence of frequencies is called a "multi-burst" which is very useful.

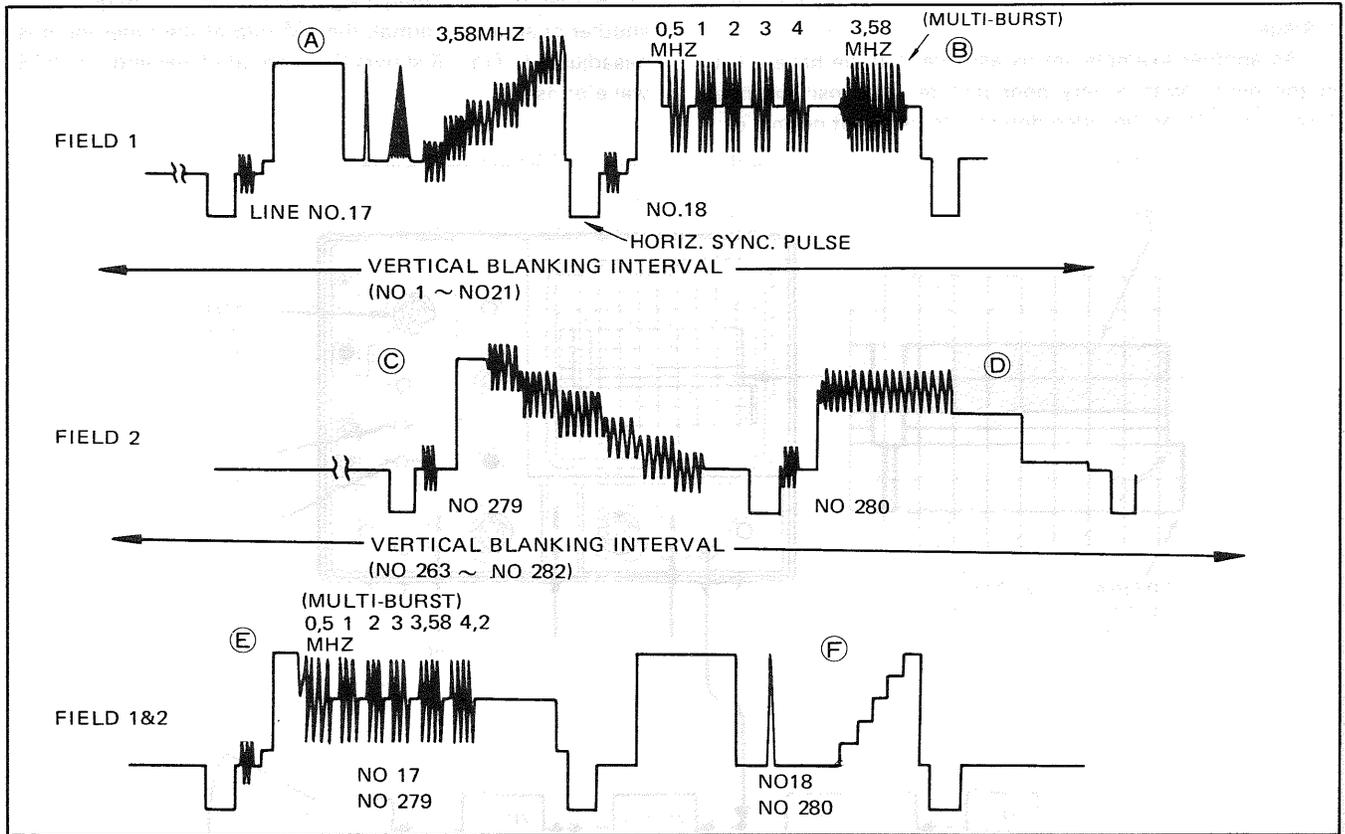


Fig. 13. VITS signal, Fields 1 and 2

The VITS other than the multi-burst signal is different depending on broadcast station. VITS staircase waveform containing a 3.58MHz burst signal is valuable to the network, but has less value to the service technician. As Field 1 is interlaced with Field 2, line 17 is followed by line 279 and line 18 is followed by line 280. The entire VITS appears at the bottom of the vertical blanking pulse and just before the first line of the video signal.

Each of the multi-burst frequencies is transmitted at equal strength. By observing the comparative strengths of these frequencies after the signal is processed through the television receiver, the frequency response of the set can be checked.

All multi-burst frequencies are transmitted at the same level, but will appear as shown in Fig. 14 even on a good color television set, due to its response curve; showing the allowable amount of attenuation for each multi-burst frequency. Remember that -6dB equals half the reference voltage (the 2.0MHz modulation should be used for reference).

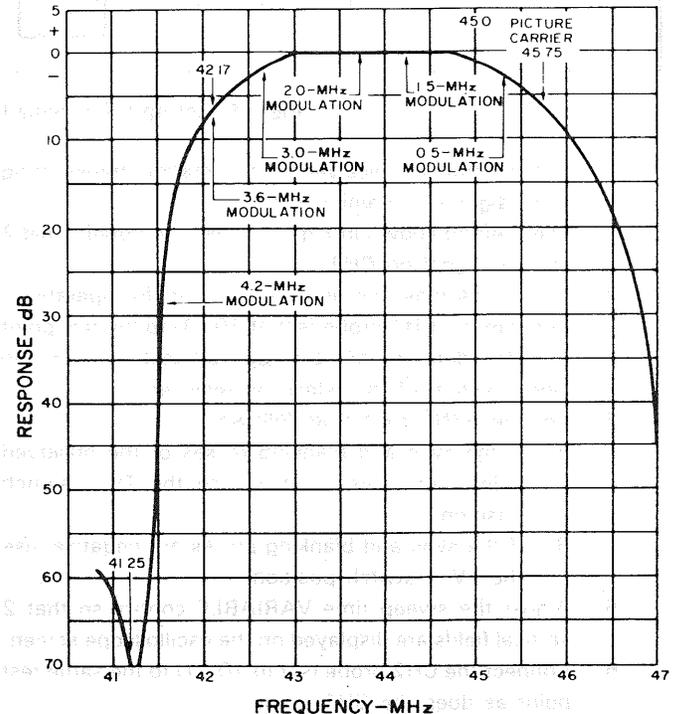


Fig. 14. Color TV IF amplifier response curve

To localize trouble, start by observing the VITS at the video detector. This will localize trouble to a point either before or after the detector. If the picture quality of each channel is different, the trouble is in the tuner or antenna system. If the picture quality is the same for all channels but the multi-burst is abnormal, then the trouble may be in the IF stage.

As another example, let us assume that we have a set on the bench with a very poor picture. Our oscilloscope shows the VITS at the video detector to be about normal ex-

cept that the burst at 2.0MHz is low compared to other burst signals. This suggests the IF trap is detuned into the passband, chopping out frequencies about 2MHz below the picture carrier frequency. Switch to another channel. If the amplifier requires realignment. If the picture quality is the same, then our reasoning is right, and if the picture quality of another channel is normal, the FM trap at the tuner input is misadjusted. Fig. 15 shows the method of viewing the VITS waveforms.

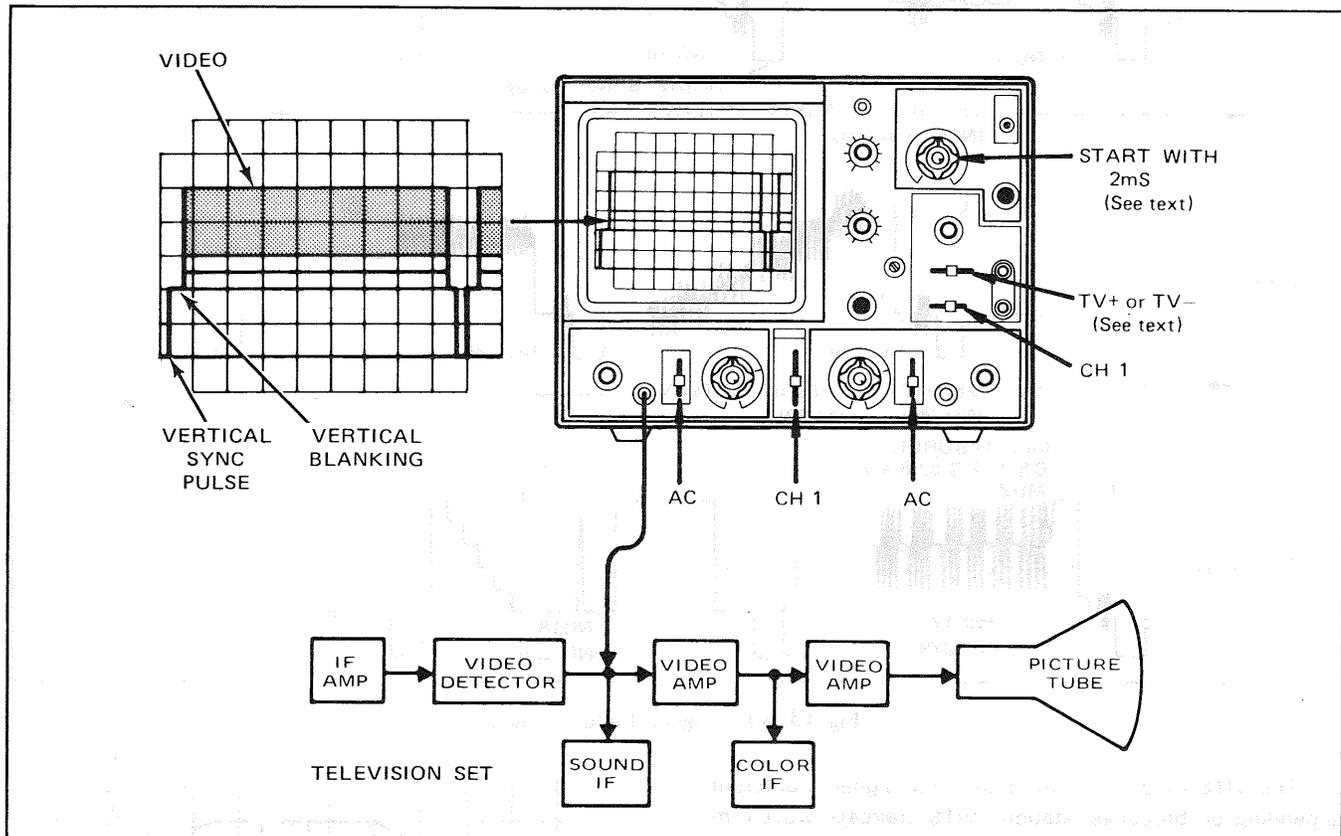


Fig. 15. Set-up for viewing fields 1 and 2 of VITS information

1. Set a color TV receiver to the station transmitting color signals containing VITS.
2. The method shown in Fig. 16 is used to obtain Field 2 vertical signal on CH1.
3. Set the oscilloscope and the receiver for operation. Connect the CH1 probe (set at 10 : 1) to the test point of video detector or other desired test point in the video section of the television receiver.
4. Set the SYNC switch as follows:
 - A. If the sync and blanking pulses of the observed video signal are positive, use the TV+ switch position.
 - B. If the sync and blanking pulses are negative, use the TV- switch position.
5. Adjust the sweep time VARIABLE control so that 2 vertical fields are displayed on the oscilloscope screen.
6. Connect the CH2 probe (set to 10 : 1) to the same test point as does the CH1 probe.
7. Set the MODE switch to DUAL position.
8. Place the sweep time VARIABLE in the CAL position.
9. Set the SWEEP TIME/DIV control to the 0.1ms position to expand the display. The VITS information will appear toward the right hand portion of the expanded waveform displays. The waveform information on each trace may appear as shown in Fig. 13. Because there is no provision for synchronizing the oscilloscope display to either of the two fields which comprise a complete vertical frame, it cannot be predicted which field display will appear on CH1 or CH2.
10. Pull the ◀▶ POSITION control outward to obtain an additional X 5 magnification. Rotate the control moving the trace to the left until the expanded VITS information appears as shown in Fig. 13. Because of the low repetition rate and the high sweep speed combination, the brightness level of the signal displays will be reduced.
11. Once the CH1 and CH2 displays have been identified

as being either Field 1 or Field 2 VITS information, the probe corresponding to the waveform display can be used for signal-tracing and troubleshooting, and the remaining probe should be left at the video detector test point to ensure that the sync signal is not interrupted. If the sync signal is interrupted, the waveform displays may be reversed because, as previously explained, there is no provision in the oscilloscope to identify either of the two vertical fields which comprise a complete frame.

SINGLE-CHANNEL APPLICATIONS

Introduction:

In addition to the dual-trace applications previously outlined, there are, of course, many servicing and laboratory applications where only single-trace or single-channel operation of the oscilloscope is required. By setting the MODE switch to CH2 and using the CH2 amplifier, many flexible operations will be achieved; and, in addition, by placing the MODE switch to SUB position (with the CH1 DC-GND-AC switch in the GND position), whatever waveform is obtained can be inverted in polarity if desired by the operator.

Television Servicing:

A triggered sweep oscilloscope is advantageous in servicing and aligning television receivers. This oscilloscope also includes several features that were incorporated to make television servicing easier observation and more comprehensive.

- * With the SYNC switch set to TV position, the SWEEP TIME/DIV control automatically selects the TV vertical sync at sweep speeds appropriate for viewing frames and TV horizontal sync at sweep speeds appropriate for viewing lines.
- * Wide bandwidth for high resolution video and high speed pulse presentation.

Single-trace Operation and Peak-to-Peak Voltage Readings:

For general troubleshooting and isolation of troubles in television receivers, the oscilloscope is an indispensable instrument. It provides a visual display of the absence or presence of normal signals. This method (signal-tracing) may be used to trace a signal by measuring several points in the signal path. As measurements proceed along the signal path, a point may be found where the signal disappears. When this happens, the source of trouble has been located.

However, the oscilloscope shows much more than the mere presence or absence of signals. It provides a peak-to-peak voltage measurement of the signal as well as presentation of waveforms. The schematic diagram or accompanying service data on the equipment being serviced usually includes waveform diagram. This waveform diagram includes the required sweep time and the normal peak-to-peak voltage. Compare the peak-to-peak voltage readings on the oscilloscope with those shown on the waveform diagram.

Composite Video Waveform Analysis:

Probably the most important waveform in television servicing is the composite waveform consisting of the video signal, the blanking pedestal signal and the sync pulses. Fig. 17 and Fig. 18 show typical oscilloscope traces when observing composite video signals synchronized with horizontal sync pulses and vertical blanking pulses. Composite video signals can be observed at various stages of the television receiver to determine whether circuits are performing normally. Knowledge of waveform makeup, the appearance of a normal waveform, and the causes of various abnormal waveforms help the technician locate and correct many problems. The technician should study such waveforms in a television receiver known to be in good operating condition, noting the waveform at various points in the video amplifier.

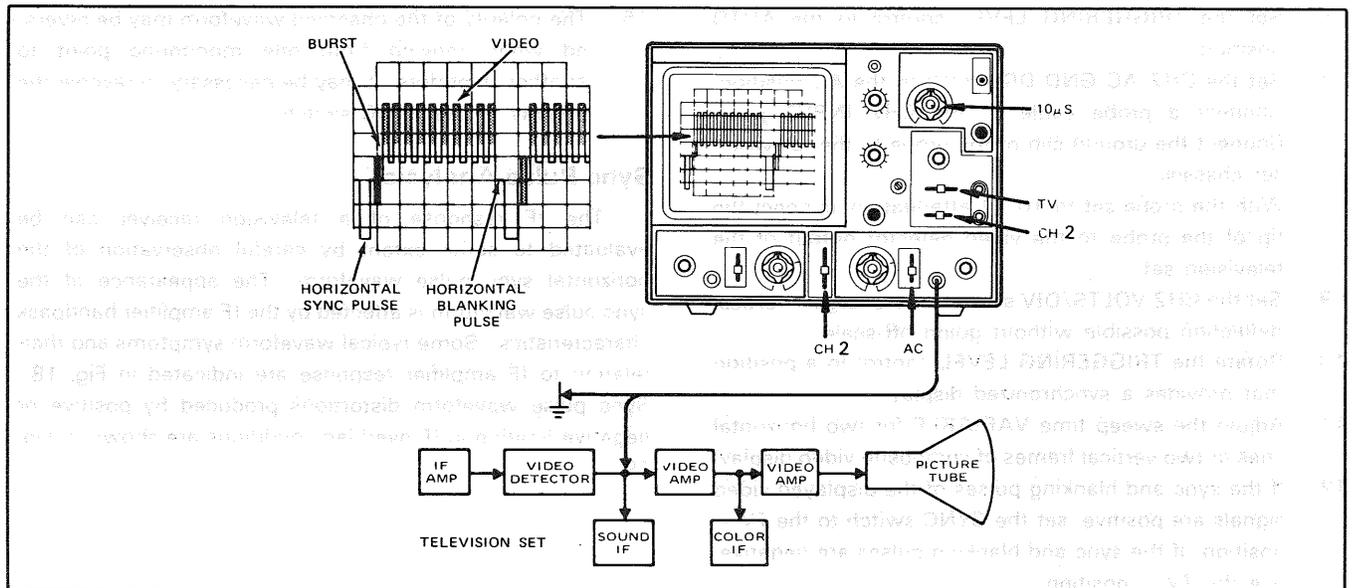


Fig. 16. Set-up for viewing horizontal fields of composite video signal

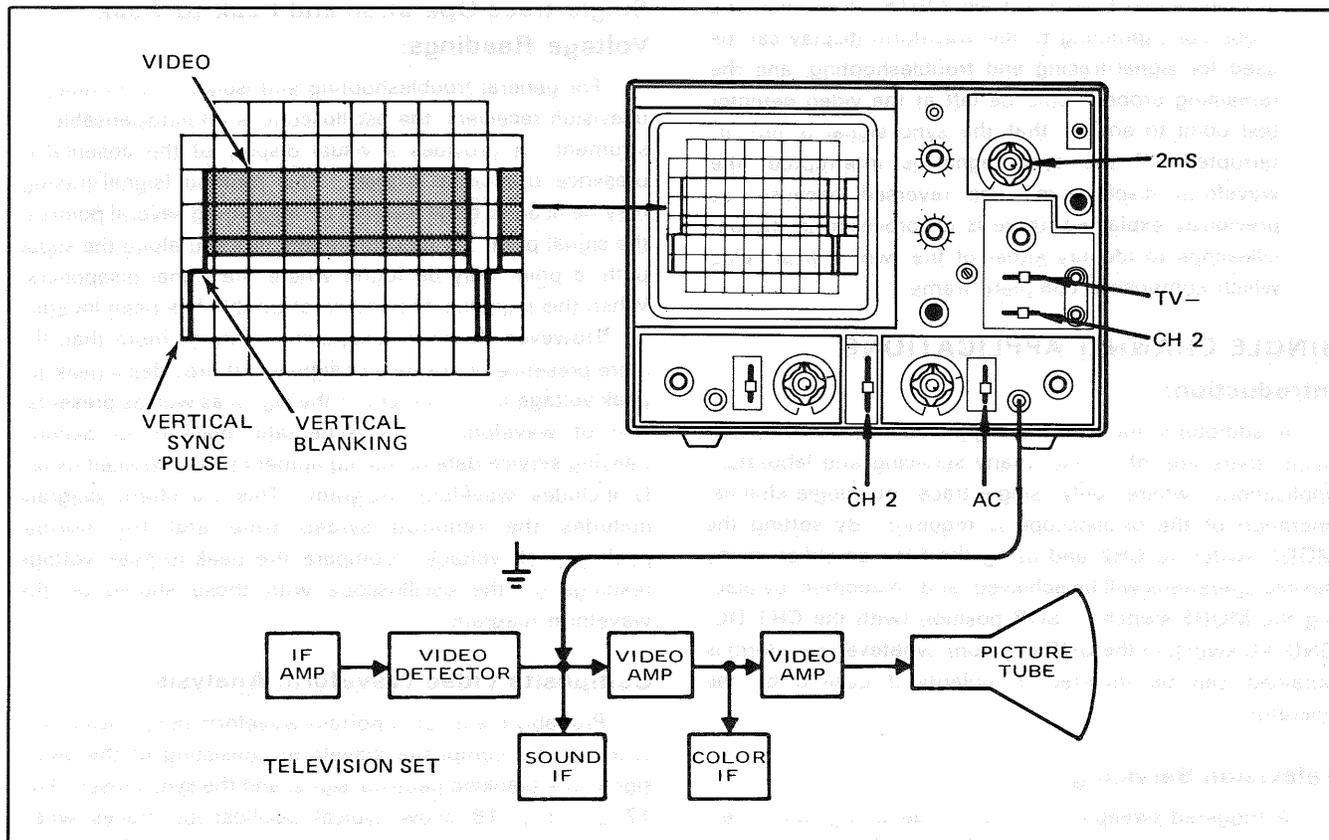


Fig. 17. Set-up for viewing *vertical* fields of composite video signal

To set up the oscilloscope for viewing composite video waveforms, use the following procedures:

1. Tune the television set to a local channel.
 2. Set the MODE switch to CH2 position.
 3. Set the SWEEP TIME/DIV switch to the $10\mu\text{s}$ position for observing TV horizontal lines or to the 2ms position for observing TV vertical frames.
 4. Set the SYNC switch to the TV+ position.
 5. Set the SOURCE switch to the CH2 position.
 6. Set the TRIGGERING LEVEL control to the AUTO position.
 7. Set the CH2 AC-GND-DC switch to the AC position.
 8. Connect a probe cable to the CH2 INPUT jack. Connect the ground clip of the probe to the television set chassis.
- With the probe set to 10 : 1 attenuation, connect the tip of the probe to the video detector output of the television set.
9. Set the CH2 VOLTS/DIV switch for the largest vertical deflection possible without going off-scale.
 10. Rotate the TRIGGERING LEVEL control to a position that provides a synchronized display.
 11. Adjust the sweep time VARIABLE for two horizontal lines or two vertical frames of composite video display.
 12. If the sync and blanking pulses of the displayed video signals are positive, set the SYNC switch to the TV+ position; if the sync and blanking pulses are negative, use the TV- position.

13. Push in the TRIGGERING LEVEL control and rotate to a position that provides a well synchronized display.
14. Adjust the INTENSITY and FOCUS controls for the desired brightness and best focus.
15. To view a specific portion of the waveform, such as the color burst, pull the ◀▶ POSITION control for X5 magnification. Rotate the same control left or right to select the desired portion of the waveform to be viewed.
16. The polarity of the observed waveform may be reversed when moving from one monitoring point to another; therefore, it may be necessary to reverse the polarity of the SYNC switch.

Sync Pulse Analysis:

The IF response of a television receiver can be evaluated to some extent by careful observation of the horizontal sync pulse waveform. The appearance of the sync pulse waveform is affected by the IF amplifier bandpass characteristics. Some typical waveform symptoms and their relation to IF amplifier response are indicated in Fig. 18. Sync pulse waveform distortions produced by positive or negative limiting in IF overload conditions are shown in Fig. 19.

CIRCUIT DEFECT	HORIZONTAL PULSE DISTORTION	OVERALL RECEIVER FREQUENCY RESPONSE	EFFECT ON PICTURE
NORMAL CIRCUIT			PICTURE NORMAL
LOSS OF HIGH FREQUENCY RESPONSE			LOSS OF PICTURE DETAIL
EXCESSIVE HIGH FREQUENCY RESPONSE, NON-LINEAR PHASE SHIFT			FINE VERTICAL BLACK & WHITE STRIATIONS FOLLOWING A SHARP CHANGE IN PICTURE SHADING
LOSS OF LOW FREQUENCY RESPONSE			CHANGE IN SHADING OF LARGE PICTURE AREAS; SHEARED PICTURE

Fig. 18. Analysis of sync pulse distortion

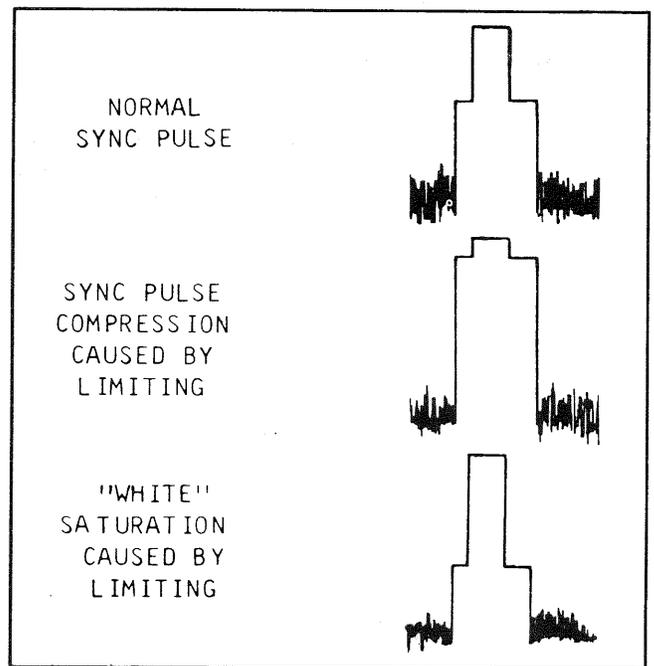


Fig. 19. Sync pulse waveforms

FM RECEIVER ADJUSTMENTS

1. Connect a sweep generator to the mixer input of the FM receiver. Set the sweep generator for a 10.7MHz center sweep.
2. Connect the sweep voltage output of the sweep generator to the CH2 input jack of the oscilloscope and set the oscilloscope controls for external horizontal sweep (SWEEP TIME/DIV to X-Y).
3. Connect the vertical input probe to the demodulator input of the FM receiver.
4. Adjust the oscilloscope vertical and horizontal gain controls for display similar to that shown in Fig. 20A.
5. Set the marker generator precisely to 10.7MHz. The marker "pip" should be in the center of the bandpass.
6. Align the IF amplifiers according to the manufacturer's specifications.
7. Move the probe to the demodulator output. The "S" curve should be displayed, and the 10.7MHz "pip" should appear in the center (see Fig. 20B). Adjust the demodulator according to the manufacturer's instructions so the marker moves an equal distance from the center as the marker frequency is amplified an equal amount from the 10.7MHz center frequency.

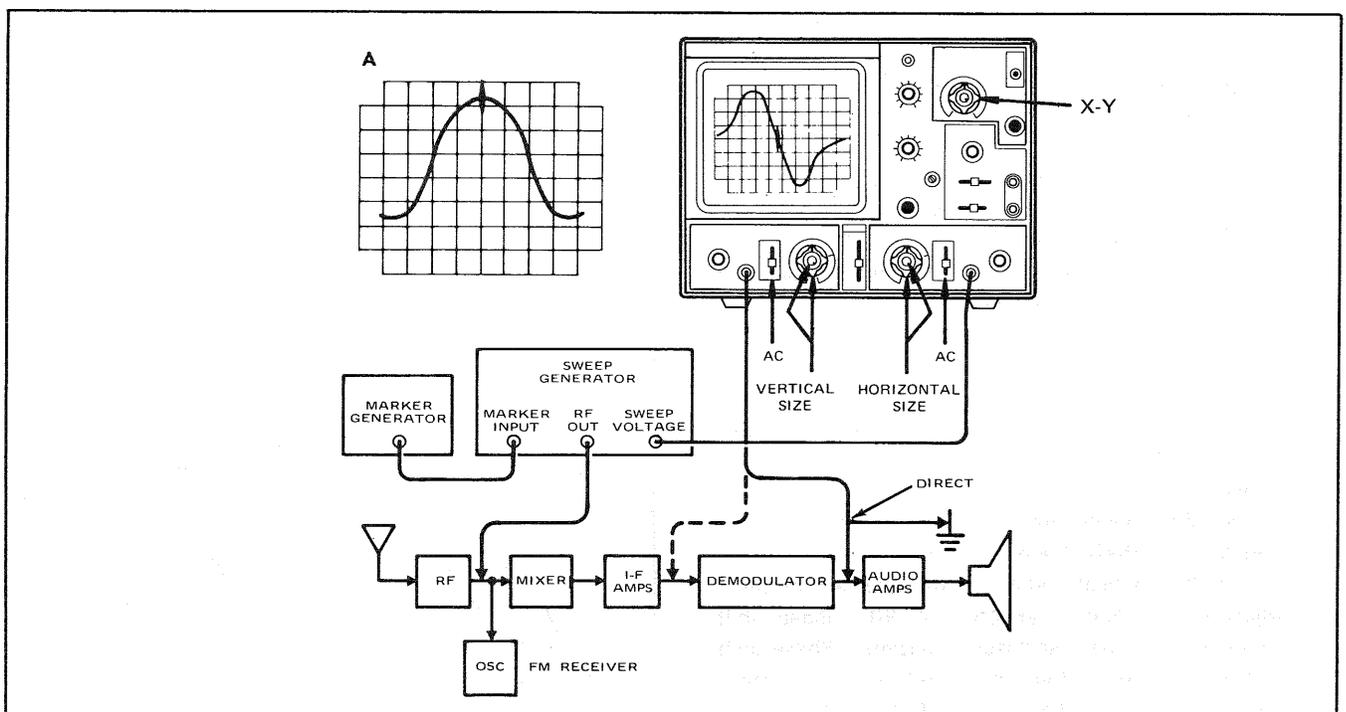


Fig. 20. Typical FM receiver alignment set-up

X-Y OPERATION APPLICATIONS

Phase Measurement:

Phase measurements may be made with an oscilloscope. Typical applications are in circuits designed to produce a specific phase shift, and measurement of phase shift distortion in audio amplifiers or other audio networks. Distortion due to non-linear amplification is also displayed in the oscilloscope waveform.

A sine wave input is applied to the audio circuit being tested. The same sine wave input is applied to the vertical input of the oscilloscope, and the output of the tested circuit is applied to the horizontal input of the oscilloscope. The amount of phase difference between the two signals can be calculated from the resulting Lissajous' waveform.

To make phase measurements, use the following procedures (refer to Fig. 21).

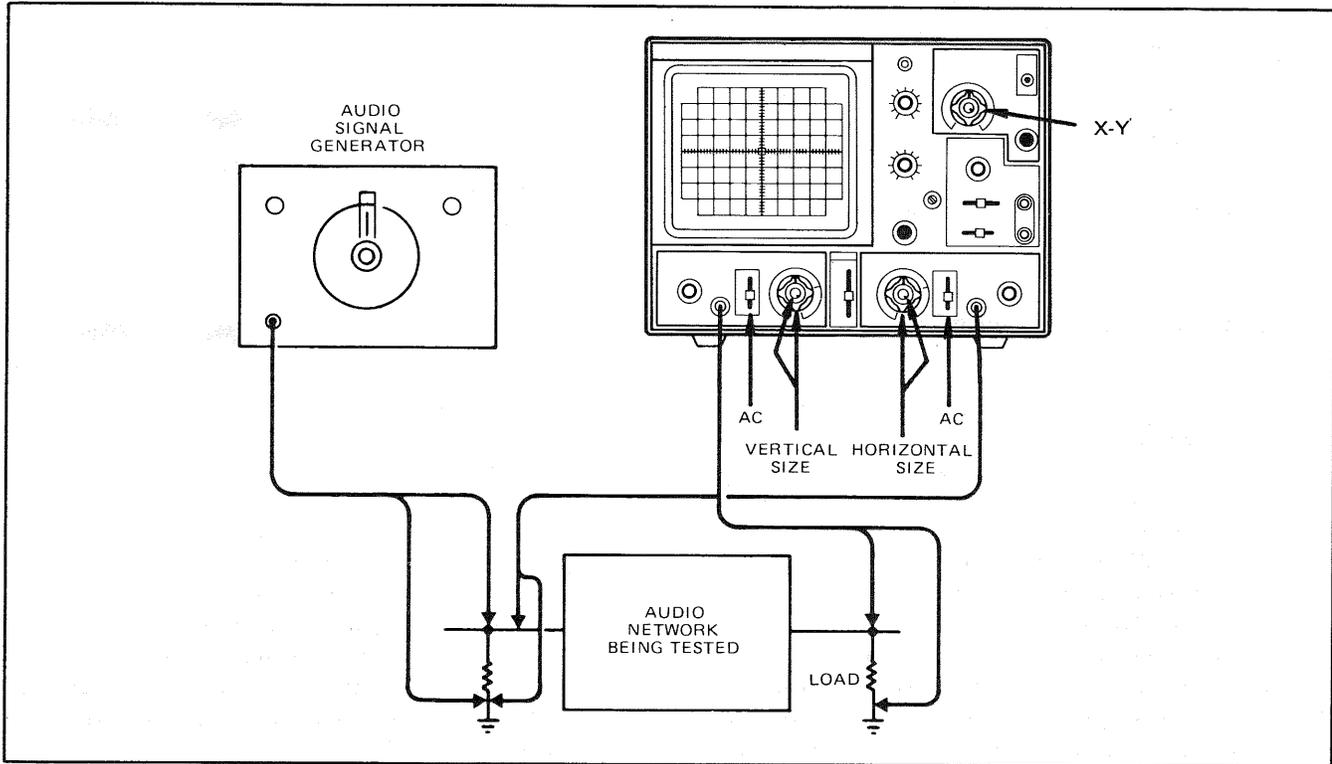


Fig. 21. Typical phase measurement alignment set-up

1. Using an audio signal generator with a pure sinusoidal signal, apply a sine wave test signal to the audio network being tested.
2. Set the signal generator output for the normal operating level of the circuit being tested. Observe the circuit's output on the oscilloscope and if the test circuit is overdriven, the sine wave display is clipped and the signal level must be reduced.
3. Connect the CH1 probe to the output of the test circuit.
4. Set the SWEEP TIME/DIV to X-Y.
5. Connect the CH2 probe to the input of the test circuit.
6. Adjust the CH1 and CH2 gain controls for a suitable viewing size.
7. Some typical results are shown in Fig. 22. If the two signals are in phase, the oscilloscope trace is a straight line. If the vertical and horizontal gain are properly adjusted, this line is at 45°. A 90° phase shift produces a circular oscilloscope pattern. Phase shift of less (or more) than 90° produces an elliptical Lissajous' pattern. The amount of phase shift can be calculated by the method shown in Fig. 23.

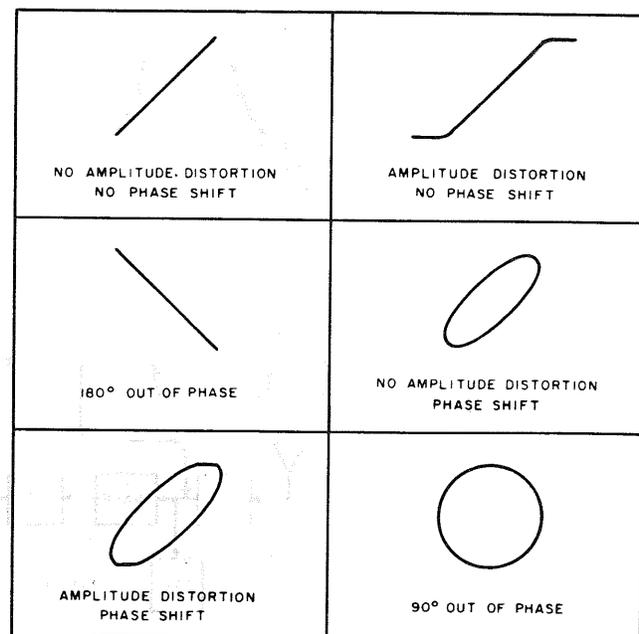


Fig. 22. Typical phase measurement oscilloscope displays

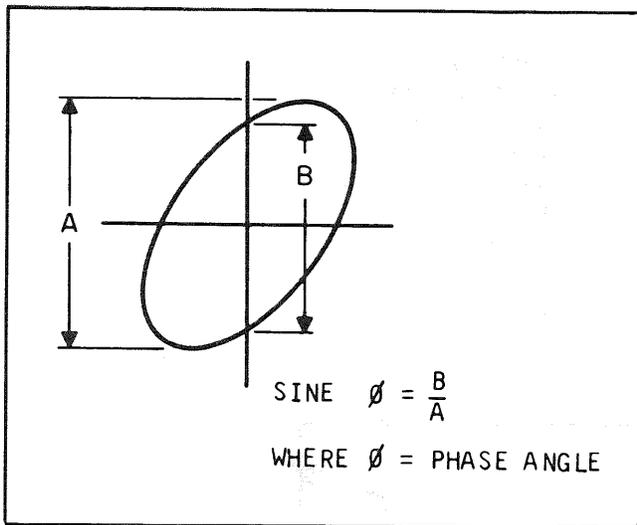


Fig. 23. Phase shift calculation

Frequency Measurement:

1. Connect the sine wave of known frequency to the CH2 input of the oscilloscope and set the SWEEP TIME/DIV control to X-Y.
2. Connect the CH1 probe to the signal to be measured.
3. Adjust the CH1 and CH2 for proper sizes.
4. The resulting Lissajous' pattern shows the ratio between the two frequencies (see Fig. 25).

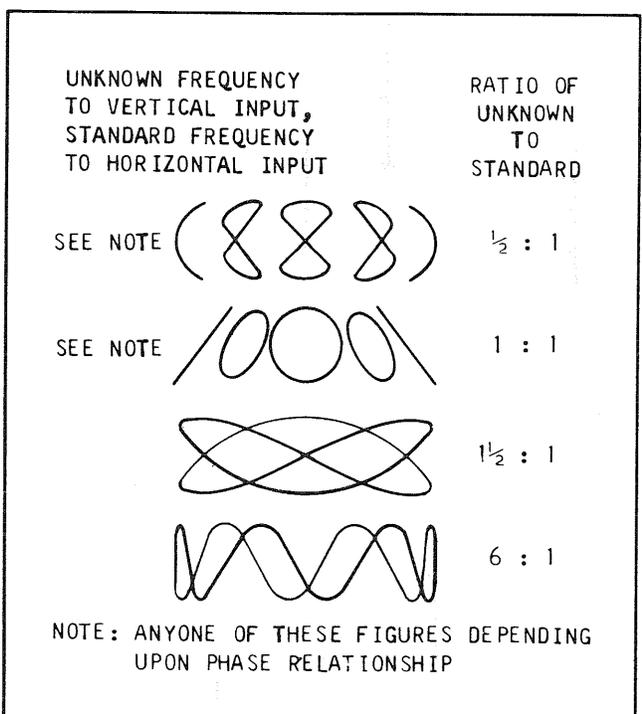


Fig. 24. Lissajous' waveforms used for frequency measurement

AMPLIFIER SQUARE WAVE TEST

Introduction:

A square wave generator and the oscilloscope can be used to display various types of distortion present in electric circuits. A square wave of a given frequency contains a large number of odd harmonics of that frequency. If a 500Hz square wave is injected into a circuit, frequency components of 1.5kHz, 2.5kHz and 3.5kHz are also provided. Since vacuum tubes and transistors are non-linear, it is difficult to amplify and reproduce a square wave which is identical to the input signal. Interelectrode capacitances, junction capacitances, stray capacitances as well as narrow band devices and transformer response are factors which prevent faithful response of a square wave signal. A well-designed amplifier can minimize the distortion caused by these limitations. Poorly designed or defective amplifiers can introduce distortion to the point where their performance is unsatisfactory.

As stated before, a square wave contains a large number of odd harmonics. By injecting a 500Hz sine wave into an amplifier, we can evaluate amplifier response at 500Hz only, but by injecting a square wave of the same frequency we can determine how the amplifier would respond to input signals from 500Hz up to the 15th or 21st harmonic.

The need for square wave evaluation becomes apparent if we realize that some audio amplifiers will be required during normal use to pass simultaneously a large number of different frequencies. With a square wave, we can evaluate the quality of input and output characteristics of a signal containing a large number of frequency components such as complex waveforms of musical instruments or voices.

The square wave output of the signal generator must be extremely flat. The oscilloscope vertical input should be set to DC as it will introduce the least distortion, especially at low frequencies. Because of the harmonic content of the square wave, distortion will occur before the upper end of the amplifier bandpass.

It should be noted that the actual response check of an amplifier should be made using a sine wave signal. This is especially important in a limited bandpass amplifier such as a voice amplifier.

The square wave signal provides a quick check of amplifier performance and will give an estimate of overall amplifier quality. The square wave also will reveal some deficiencies not readily apparent when using a sine wave signal. Whether a sine wave or square wave is used for testing the amplifier, it is important that the manufacturer's specifications on the amplifier be known in order to make a better judgement of its performance.

Testing Procedure (refer to Fig. 25):

1. Connect the output of the square wave generator to the input of the amplifier being tested.
2. Connect the CH2 probe of the oscilloscope to the output of the amplifier.
3. If the DC component of the amplifier output is low, set the AC-GND-DC switch to DC position to allow both the AC and DC components to be viewed. However, the AC position may be used to observe the AC component only, though this will reduce the audio frequency content of less than 5Hz.
4. Adjust the vertical gain controls for a convenient viewing height.
5. Adjust the sweep time controls for one cycle of square wave display on the screen.
6. For a close-up view of a portion of the square wave, use X5 magnification.

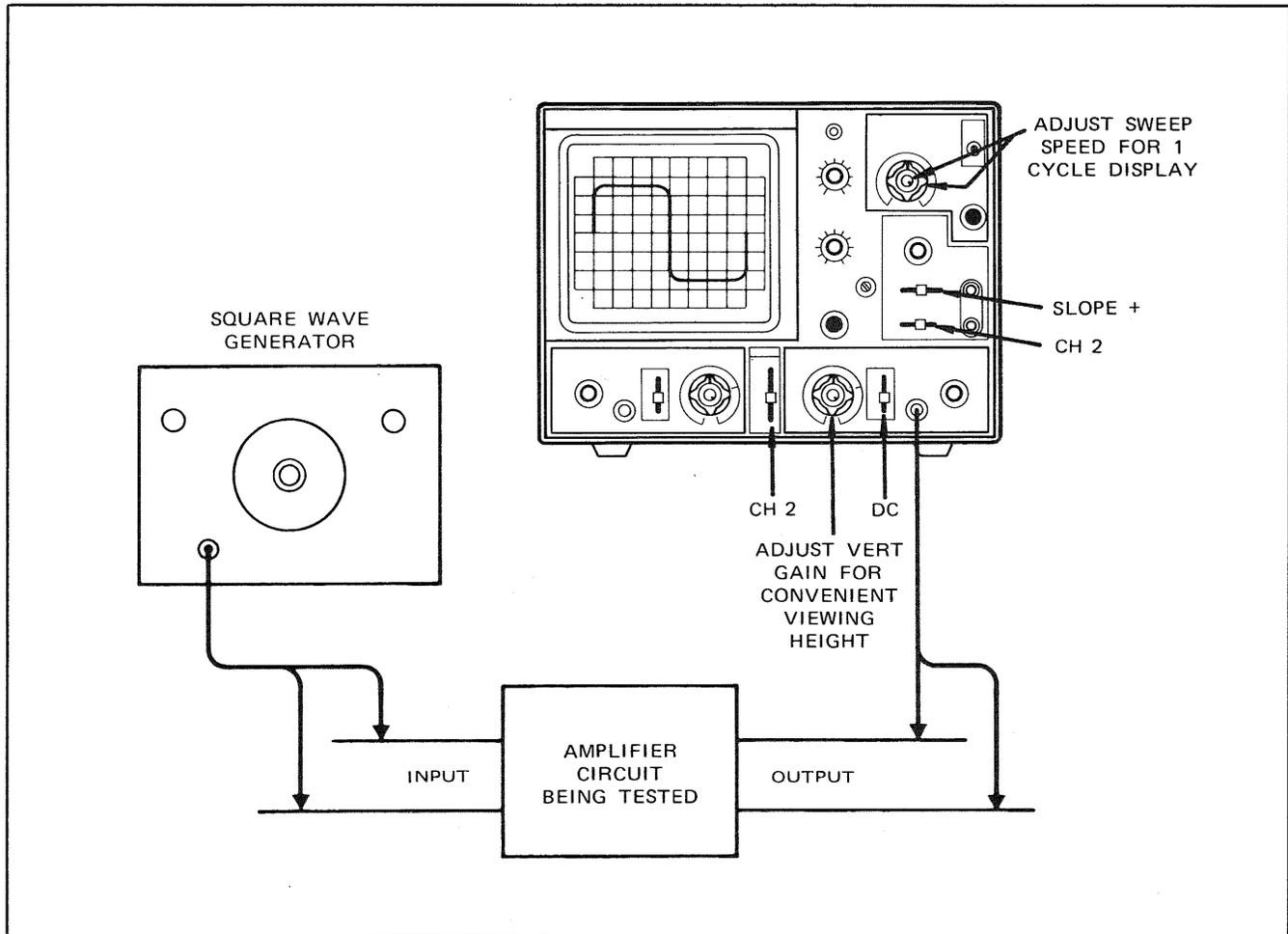


Fig. 25. Equipment set-up for square wave testing of amplifiers

Analysing the Waveforms:

The short rise time which occurs at the beginning of the half-cycle is created by the in-phase sum of the medium and high frequency sine wave components. The same holds true for the drop time. The reduction in high frequency components should produce a rounding of the square corners at all four points of one square wave cycle (see Fig. 26).

Distortion can be classified into the following three categories:

1. The first is frequency distortion and refers to the change in the amplitude of a complex waveform. In other words, the introduction in an amplifier circuit of resonant networks or selective filters created by combination of reactive components will create peaks or dips in an otherwise flat frequency response curve.

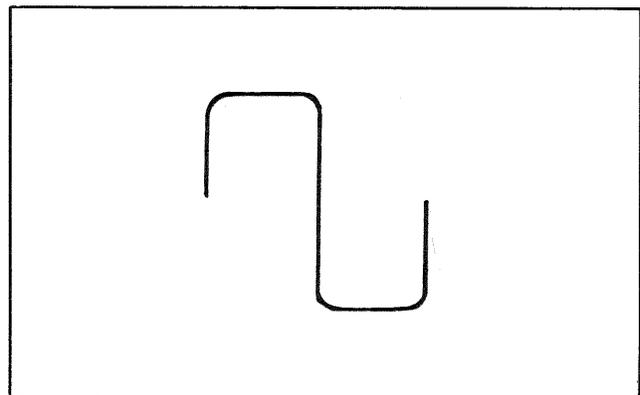


Fig. 26. Square wave response with high frequency loss

2. The second is non-linear distortion and refers to a change in waveshape produced by application of the waveshape to non-linear elements such as vacuum tubes, an iron core transformer or a clipper network.
3. The third is delay or phase distortion, which is distortion produced by a shift in phase between some components of a complex waveform.

In actual practice, a change in amplitude of a square wave component is usually caused by a frequency selective network which includes capacity, inductance or both. The presence of the C or L introduces a difference in phase angle between components, creating phase distortion or delay distortion. Therefore, in square wave testing of practical circuitry, we will usually find that the distorted square wave includes a combination of amplitude distortion and phase distortion.

In a typical wide band amplifier, a square wave check reveals many distortion characteristics of the circuit. The response of an amplifier is indicated in Fig. 27, revealing poor low-frequency response along with the overcompensated high-frequency boost. The response of 100Hz square wave applied to the amplifier will appear as in Fig. 28A. This figure indicates satisfactory medium frequency response (approximately 1kHz to 2kHz) but shows poor low frequency response. Next, a 1kHz square wave applied to the input of the amplifier will appear as in Fig. 28B. This figure displays good frequency response in the region of 1000 to 4000Hz but reveals a sharp rise at the top of the leading edge of the square wave because of overcompensation at the frequencies of more than 10kHz.

As a rule of thumb, it can be safely said that a square wave can be used to reveal response and phase relationships up to the 15th or 20th odd harmonic or up to approximately 40 times the fundamental of the square wave. It is seen that wide-band circuitry will require at least two frequency check points to correctly analyze the entire bandpass.

In the case illustrated by Fig. 27, a 100Hz square wave will encompass components up to about 4kHz. To analyze above 4kHz and beyond 10,000Hz, a 1kHz square wave should be used.

Now, the region between 100Hz and 4000Hz in Fig. 28 shows a rise from poor low-frequency (100Hz to 1kHz) response to a flattening out from beyond 1000 and 4000Hz. Therefore, we can expect that the higher frequency components in the 100Hz square wave will be relatively normal in amplitude and phase but that the low-frequency components "B" in this same square wave will be modified by the poor low-frequency response of this amplifier (see Fig. 28).

If the amplifier were such as to only depress the low frequency components in the square wave, a curve similar to Fig. 29 would be obtained. However, reduction in amplitude of the components is usually caused by a reactive element, causing, in turn, a phase shift of the components, producing the tilt as shown in Fig. 28A.

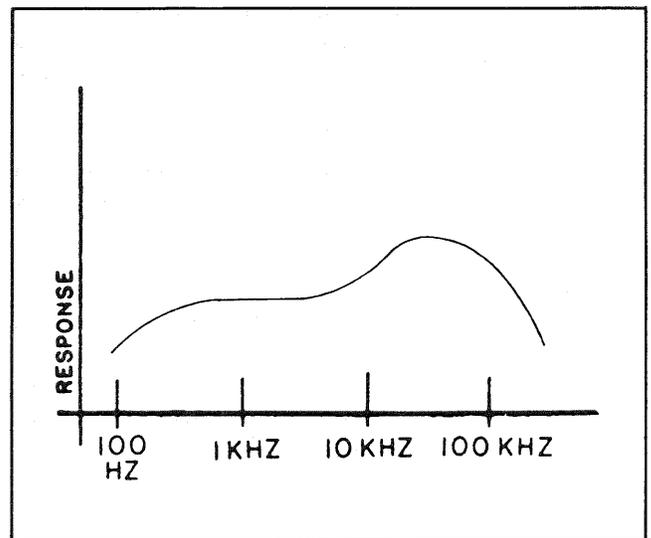


Fig. 27. Response curve of amplifier with poor low and high ends

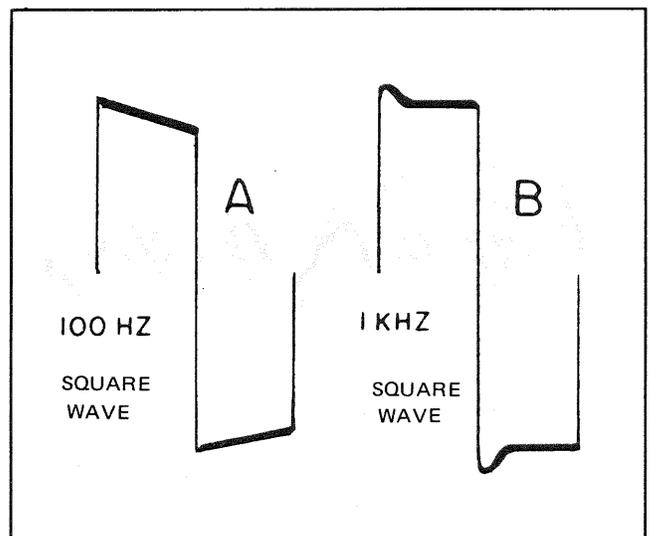


Fig. 28. Resultant 100 Hz and 1 kHz square waves from amplifier in Fig. 45

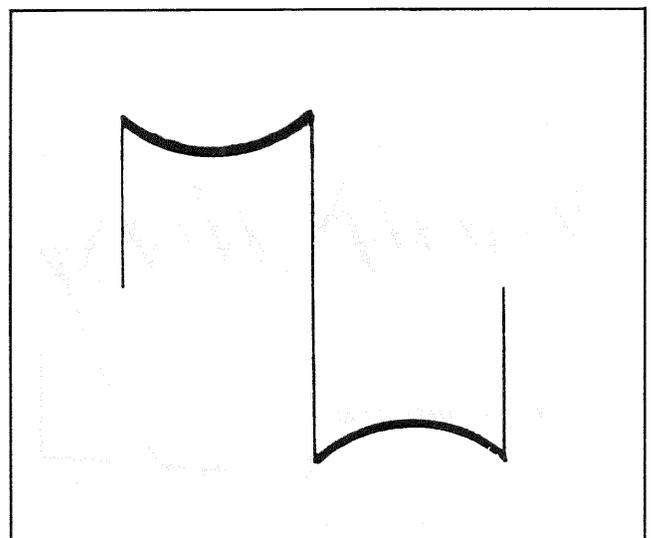


Fig. 29. Reduction of square wave fundamental frequency component in a tuned circuit

Fig. 30 shows a graphical development of a similarly tilted square wave. The tilt is seen to be caused by the strong influence of the phase-shifted 3rd harmonic. It also becomes evident that very slight shifts in phase are quickly shown up by tilt in the square wave.

Fig. 31 indicates the tilt in square wave produced by a 10° phase shift of a low-frequency element in a leading direction. Fig. 32 indicates a 10° phase shift in a low frequency component in a lagging direction. The tilts are opposite in the two cases because of the difference in polarity of the phase angle in the two cases that can be checked through algebraic addition of components.

Fig. 33 indicates low-frequency components which have been reduced in amplitude and shifted in phase. It will be noted that these examples of low-frequency distortion are characterized by a change in shape of the flat portion of the square wave.

Fig. 28B shows a high-frequency overshoot produced by rising amplifier response at high frequencies. It should

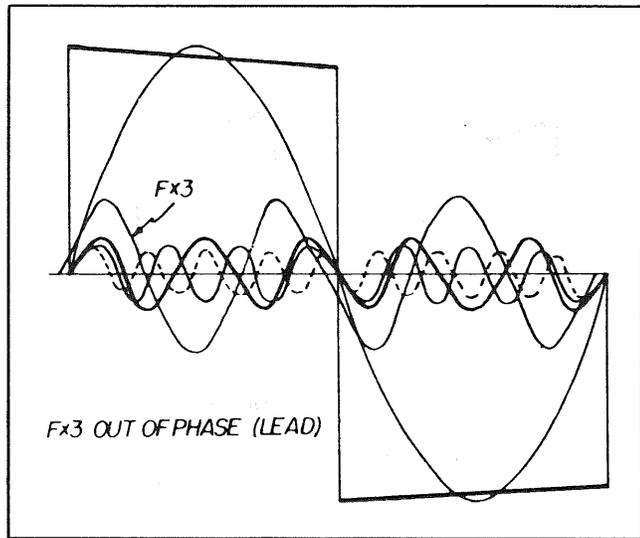


Fig. 30. Square wave tilt resulting from 3rd harmonic phase shift

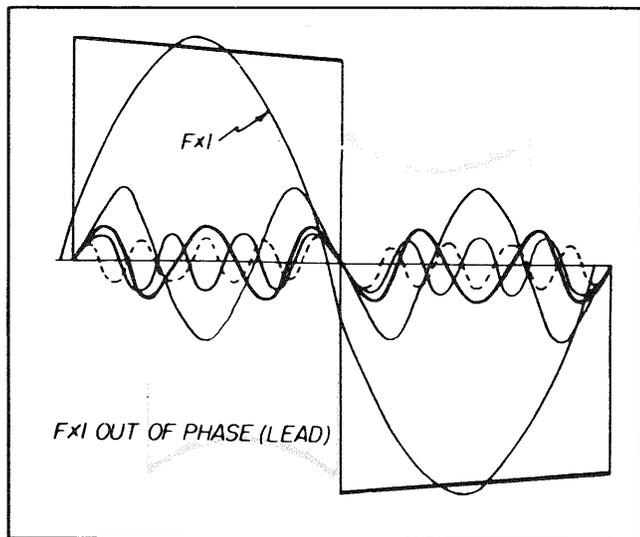


Fig. 31. Tilt resulting from phase shift of fundamental frequency in a leading direction

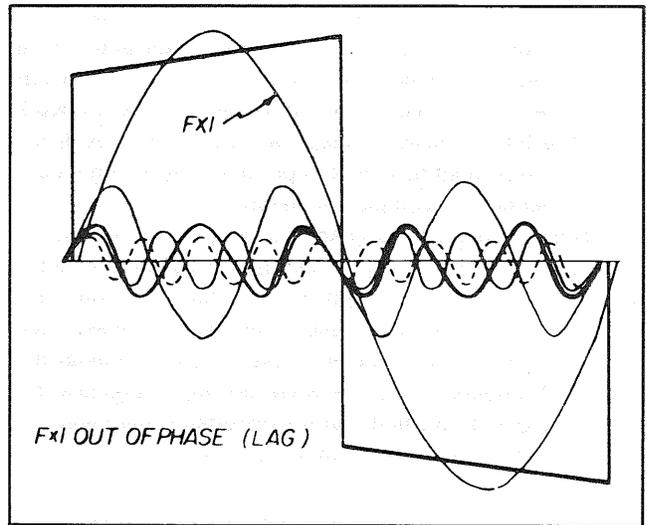


Fig. 32. Tilt resulting from a phase shift of fundamental frequency in a lagging direction

again be noted that this overshoot makes itself evident at the top of the leading edge of the square wave. The sharp rise of the leading edge is created by the summation of a large number of harmonic components. If an abnormal response occurs at high frequencies, the high frequency components in the square wave will be amplified more than the other components creating a higher algebraic sum along the leading edge.

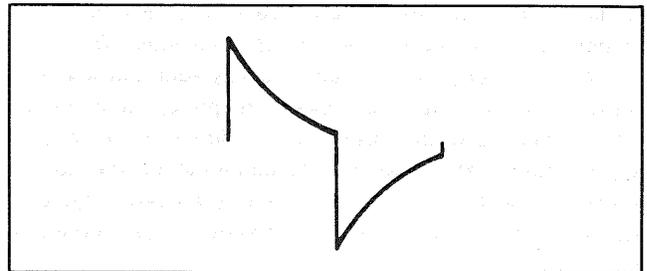


Fig. 33. Low frequency component loss and phase shift

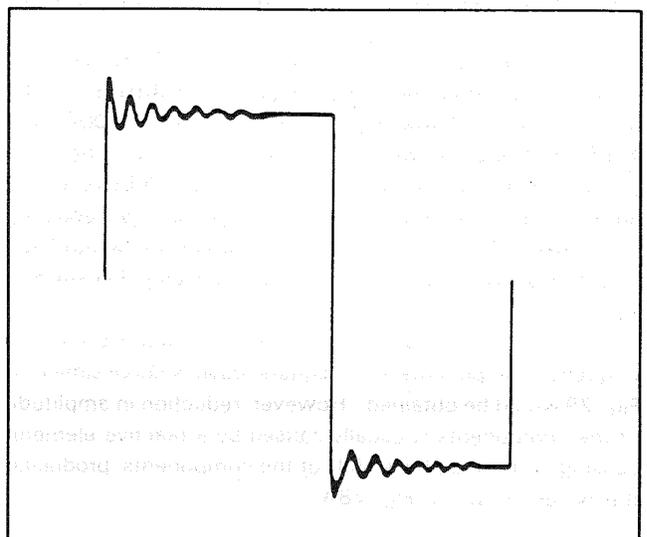


Fig. 34. Effect of high-frequency boost and poor damping

Fig. 34 indicates high-frequency boost in an amplifier accompanied by a lightly damped "shock" transient. In this case, the sudden transition in the square wave potential from a sharply rising, relatively high frequency voltage, to a level value of low frequency voltage, supplies the energy for oscillation in the resonant network. If this network in the amplifier is reasonably heavily damped, then a single cycle transient oscillation may be produced as indicated in Fig. 35.

Fig. 36 summarizes the preceding explanations and serves as a handy reference.

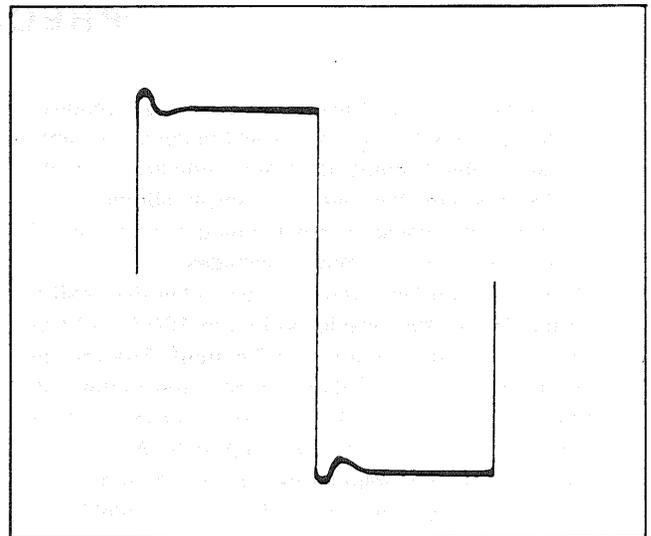


Fig. 35. Effect of high-frequency boost and good damping

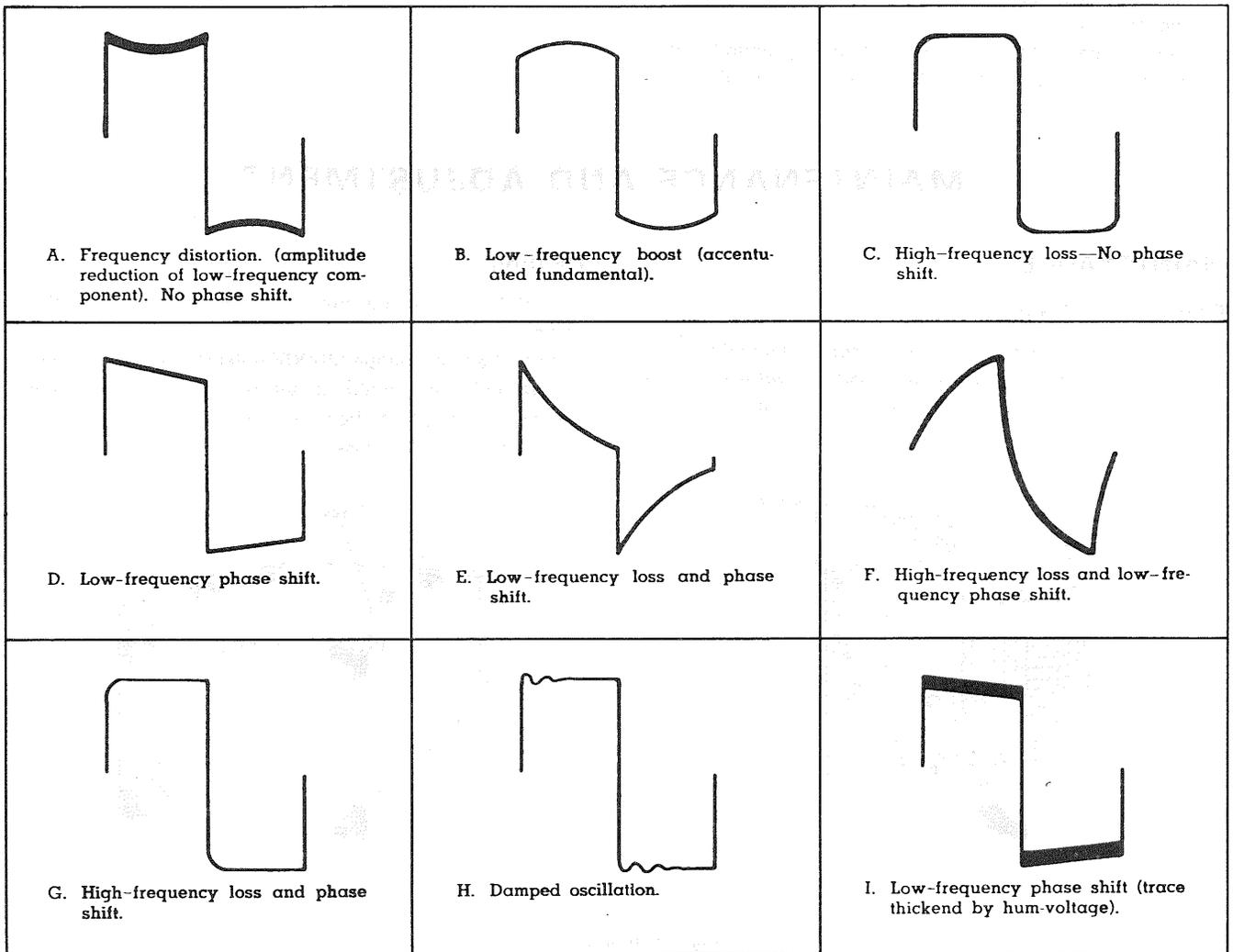


Fig. 36. Summary of waveform analysis for square wave testing of amplifiers

PRECAUTIONS

1. Do not use the unit in any of the following locations:
 - * Places where the unit is exposed to direct sunlight.
 - * Places where temperature and humidity are high.
 - * Places where there are mechanical vibration.
 - * Places near equipment generating strong lines of magnetic force or impulse voltages.
2. When operating the unit on voltages other than 240V, set the AC voltage selector switch to 100V, 117V or 220V according to your local AC current. The voltage selector switch is located on the rear panel of the unit. When operating on 100V or 117V, remove the 0.3A fuse and replace it with one rated at 0.7A.
3. Do not apply input voltages exceeding their maximum ratings. The input voltage to the vertical amplifier is up to 300V (DC + AC peak), the input for EXT TRIG is up to 50V (DC + AC peak), and the input to Z AXIS is up to 50V (DC + AC peak).
4. Do not increase the brightness of the CRT unnecessarily.
5. Do not leave the oscilloscope for a long period with bright spot displayed on CRT. Reduce the brightness and soften the focus.
6. For X-Y operation, use the PULL X5 MAG switch in the PUSH position. If it is set in the PULL position, noise may appear in the waveform.

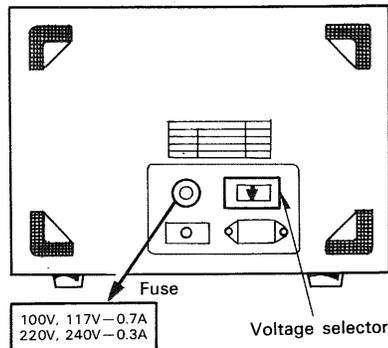


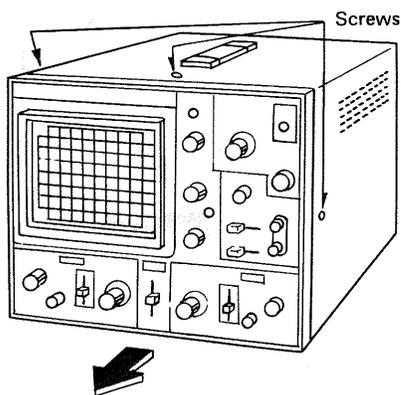
Fig. 37.

MAINTENANCE AND ADJUSTMENT

MAINTENANCE

Removal of Case

1. Remove the 5 screws from the top, sides and bottom of the case using a "cross" head screwdriver.
2. The chassis can then be readily removed from the case.



Caution

Before removing the case, be sure to turn off the power. Note that a high voltage (2000V max) is present on the CRT socket and the printed circuit board. Keep your hand, screwdriver, etc. away from any part carrying a high voltage after removal of the case.

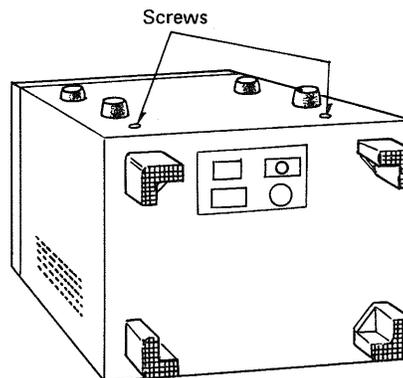


Fig. 38. Removal of Case

ADJUSTMENT

Observe the following before making adjustments

The oscilloscope is factory adjusted prior to shipment. If readjustment becomes necessary, the following points should be observed.

1. Check the power supply for correct voltage.
2. For adjustments, use a well insulated screwdriver.
3. Before marking adjustments, be sure to turn on the power and wait until the unit is stabilized.
4. For adjustments, follow the procedures described below.
5. If special test instruments are required for adjustments, contact Trio's service station.

Adjustment of Power Supply and CRT Circuits

1. Adjustment of low power voltage (Fig. 39).
Adjust VR309 so that 195V appears on the No. 1 pin of the connector on the same circuit board.
Next, check that voltages on No. 2, 3 and 5 pins of P204 are +5V, -10V and +10V, respectively.
2. Adjustment of high power voltage (Fig. 39).
* Connect a DC voltmeter of high input impedance (more than 100M-ohm) to the CRT socket at No. 1, 7 or 14 pin.
* Adjust VR306 to obtain a high voltage of -1.9 kV.
3. Intensity adjustment (Fig. 39).
* Pull the PULL AUTO knob to display a trace on CRT.
* Adjust VR307 so that the trace disappears at 9~11 o'clock position of the brightness adjustment knob.
4. Blanking voltage adjustment (Fig. 39).
Adjust TC302 so that the brightness at the sweep starting point is the same as the brightness at other points (SWEEP TIME/DIV in 0.5 μ position).
Finally, adjust the spot with FOCUS and ASTIG.

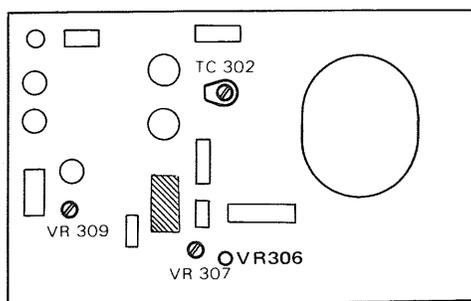


Fig. 39.

Calibreton diagram, power supply board.

5. CRT trace angle adjustment.
Adjust the TRACE ROTATION (front panel) until the trace is aligned with the horizontal line marked on the CRT scale.

Adjustment of Vertical Circuit

1. CRT Center adjustment (Fig. 40).
With the terminals TP101 and TP102 shorted, adjust VR105 until the trace comes in the center of CRT.
2. VARIABLE ATT DC BAL adjustment
* Turn the vertical attenuator VARIABLE (6) [(9) for CH2] fully counterclockwise.
* Turn the \blacktriangle POSITION (1) [(12) for CH2] until the trace is centered on the scale.
* Turn the VARIABLE fully clockwise. If, at this time, the trace shifts is position, adjust the DC BAL (2) [(13) for CH2] until the trace is positioned on the center horizontal line of the scale.
* Repeat steps (2), (3) and (4) until the trace remains stationary even when THE VARIABLE (6) is turned.
3. STEP ATT DC BAL Adjustment (Fig. 40).
* Turn the \blacktriangle POSITION (1) [(12) for CH2] until the trace is centered on the scale at 10 mV range of VOLTS/DIV.
* Next, turn the VOLTS/DIV to 20 mV range. If, at this time, the trace shifts is position, adjust the VR105 [VR109 for CH2].
* Perform the same adjustment at the 50 mV range. For adjustment at 50 mV range, use VR106 [VR108 for CH2].

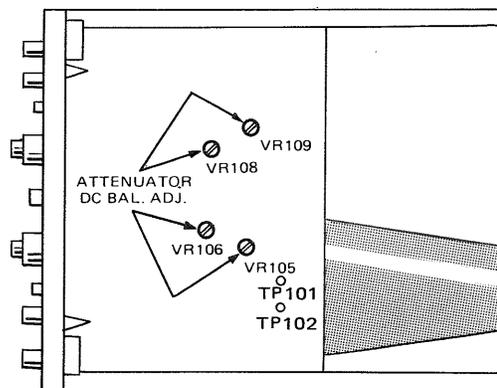


Fig. 40.

Calibration diagram, vertical amplifier board.

Horizontal Circuit Adjustment

1. \blacktriangle POSITION adjustment

To adjust the horizontal position of waveform under the normal sweep condition, proceed as follows:

With the \blacktriangle POSITION set to its mechanical center position, adjust VR206 (POS ADJ) so that the waveform starts at the left end of the scale.

2. X POSITION adjustment

To adjust the horizontal position of the waveform when the SWEEP TIME/DIV is in the X-Y position, perform the same adjustment and then adjust VR205 so that the bright spot comes to the center of the scale.

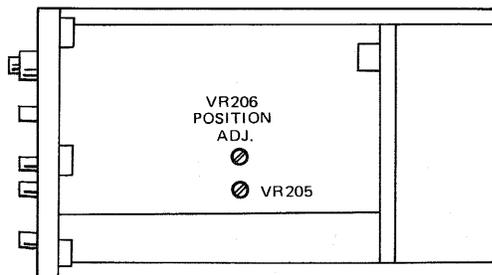
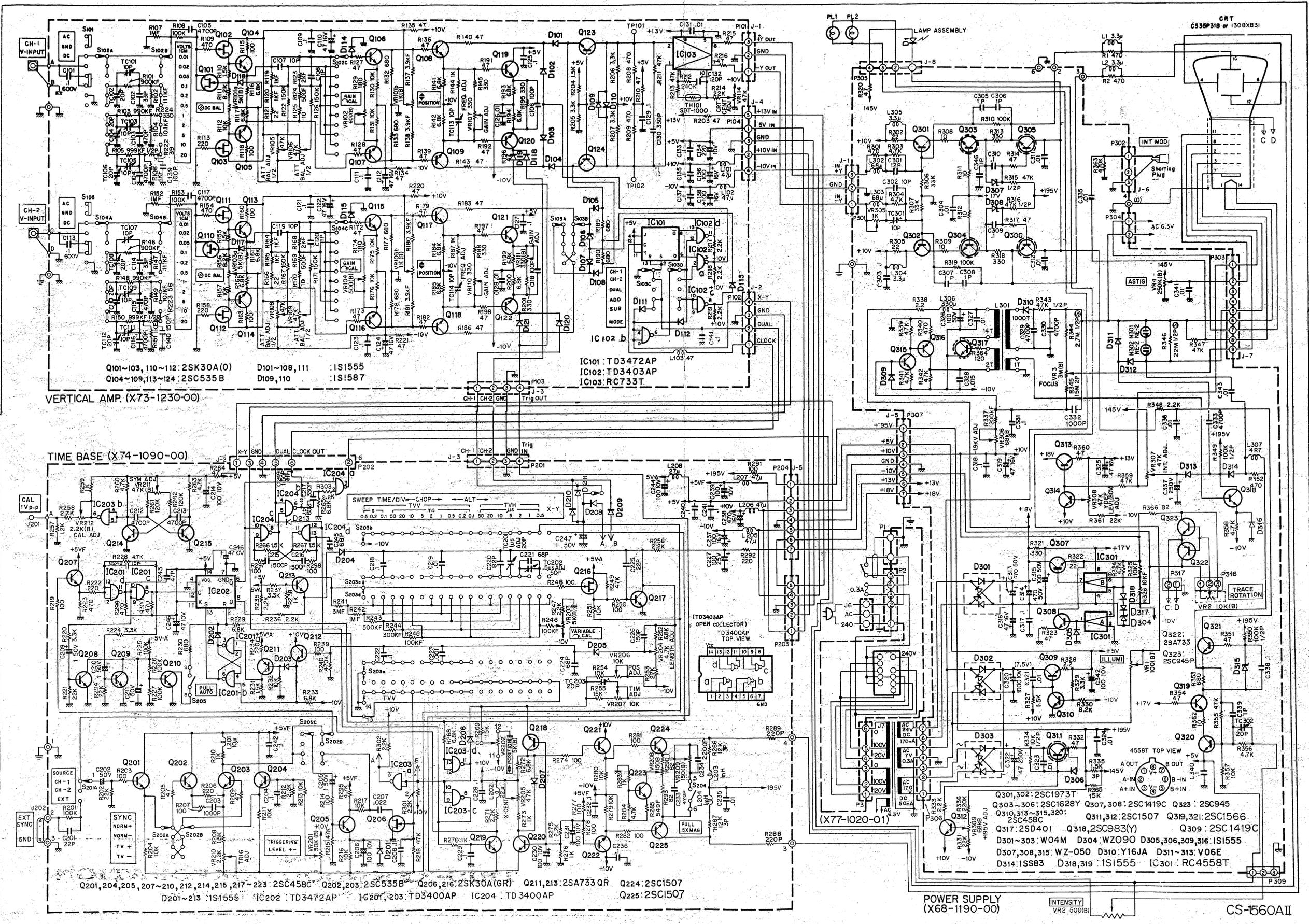


Fig. 41.

Calibration diagram, horizontal amplifier board.

SCHEMATIC DIAGRAM



Q101~103, 110~112: 2SK30A(O) D101~108, 111 : IS1555
 Q104~109, 113~124 : 2SC535 B D109, 110 : IS1587

VERTICAL AMP (X73-1230-00)

TIME BASE (X74-1090-00)

Q201, 204, 205, 207~210, 212, 214, 215, 217~223: 2SC458C Q202, 203: 2SC535B Q206, 216: 2SK30A(GR) Q211, 213: 2SA733 QR Q224: 2SC1507
 D201~213: IS1555 IC202: TD3472AP IC203: TD3400AP IC204: TD3400AP Q225: 2SC1507

POWER SUPPLY (X68-1190-00)

INTENSITY VR2 500(B)

CS-1560AII

A product of
TRIO-KENWOOD CORPORATION

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