



LS4558N

# LINEAR INTEGRATED CIRCUITS

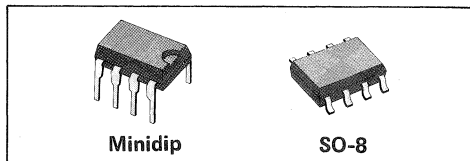
## PRELIMINARY DATA

### DUAL HIGH PERFORMANCE OPERATIONAL AMPLIFIER

- SINGLE OR SPLIT SUPPLY OPERATION
- LOW POWER CONSUMPTION
- HIGH UNITY GAIN BANDWIDTH
- NO CROSSOVER DISTORTION
- NO POP NOISE
- SHORT CIRCUIT PROTECTION
- HIGH CHANNEL SEPARATION

The LS4558N is a high performance dual operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high gain-bandwidth

products. The circuit presents very stable electrical characteristics over the entire supply voltage range and the specially designed input stage allow the LS4558N to be used in **low noise audio signal processing application**. The optimized class AB output stage completely eliminates crossover, distortion, under any load conditions, has large source and sink capacity and is short circuit protected.



### ABSOLUTE MAXIMUM RATINGS

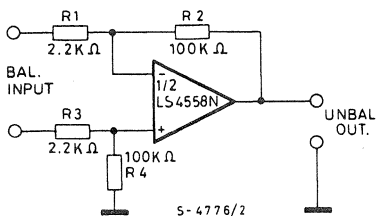
$V_s$	Supply voltage	$\pm 18$	V
$V_i$	Input voltage	$\pm V_s$	V
$V_i$	Differential input voltage	$\pm (V_s - 1)$	V
$P_{tot}$	Power dissipation at $T_{amb} = 70^\circ\text{C}$	665	mW
$T_{op}$	Operating temperature	400	mW
$T_j$	Junction temperature	0 to 70	$^\circ\text{C}$
$T_{stg}$	Storage temperature	150	$^\circ\text{C}$
		-55 to 150	$^\circ\text{C}$

Minidip  
Micropackage

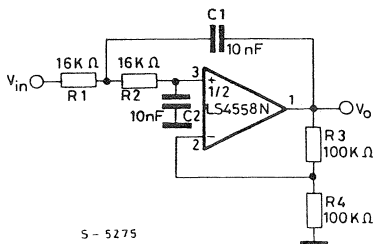
**ORDERING NUMBER:** LS 4558 NB (Minidip)  
LS 4558 NM (Micropackage)

### TYPICAL APPLICATIONS:

Balanced input audio preamplifier



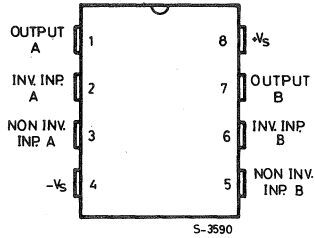
DC coupled low-pass active filter  
( $f = 1\text{KHz}$ ,  $G_v = 6\text{dB}$ )



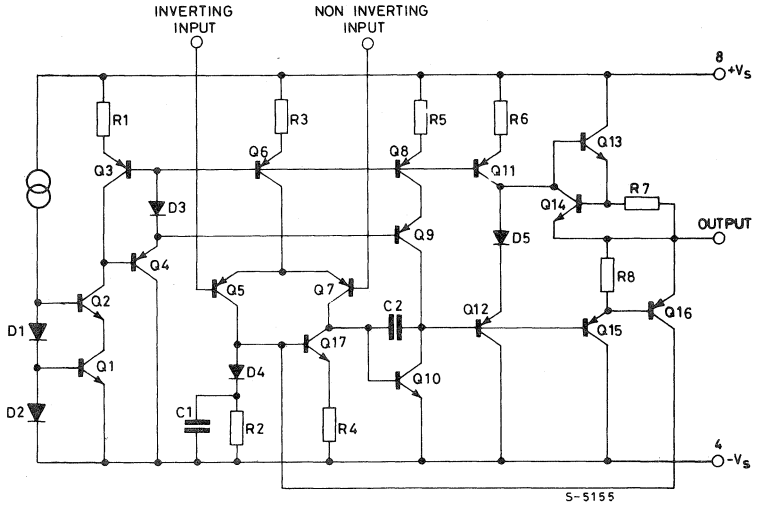


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### CONNECTION DIAGRAM (top view)



### SCHEMATIC DIAGRAM (one section)



### THERMAL DATA

	Minidip	SO-8
$R_{th j-amb}$ Thermal resistance junction-ambient	120 °C/W	200 °C/W

**ELECTRICAL CHARACTERISTICS** ( $V_s = \pm 15V$ ,  $T_{amb} = 25^\circ C$ , unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
$I_s$ Supply current (*)			1	2	mA
$I_b$ Input bias current			50	500	nA
	$T_{min} < T_{op} < T_{max}$			800	nA
$R_i$ Input resistance	$f = 1 \text{ KHz}$	0.3	1		$M\Omega$
$V_{os}$ Input offset voltage	$R_g \leq 10 \text{ K}\Omega$		0.5	5	mV
	$R_g \leq 10 \text{ K}\Omega$ $T_{min} < T_{op} < T_{max}$			7.5	mV
$I_{os}$ Input offset current			20	200	nA
	$T_{min} < T_{op} < T_{max}$			500	nA
$I_{sc}$ Output short circuit current			23		mA
$G_v$ Large signal open loop voltage gain	$R_L = 2 \text{ K}\Omega$	86	100		dB
B Gain-bandwidth product	$f = 20 \text{ KHz}$	2	3		MHz
$e_N$ Total input noise voltage	$f = 1 \text{ KHz}$ $R_g = 50\Omega$ $R_g = 1 \text{ K}\Omega$ $R_g = 10 \text{ K}\Omega$		8 10 18	15	$\frac{nV}{\sqrt{Hz}}$
$e_N$ Popcorn noise	$B = 1 \text{ Hz to } 1 \text{ KHz}$ $R_g = 10 \text{ K}\Omega$ $t = 10 \text{ sec}$			10	$\mu V$ peak
d Distortion	$G_v = 20 \text{ dB}$ $V_o = 2 \text{ Vpp}$ $R_L = 2 \text{ K}\Omega$ $f = 1 \text{ KHz}$		0.03		%
$V_o$ Output voltage swing	$R_L = 2 \text{ K}\Omega$		$\pm 13$		V
$V_o$ Large signal voltage swing	$R_L = 10 \text{ K}\Omega$ $f = 10 \text{ KHz}$		28		Vpp
Transient response	Rise time Overshoot	$V_i = 20 \text{ mV}$ $C_L = 100 \text{ pF}$ $R_L = 2 \text{ K}\Omega$	0.13		$\mu S$
			5		%
SR Slew rate	unity gain $R_L = 2 \text{ K}\Omega$	0.8	1.5		$V/\mu s$
CMR Common mode rejection	$V_i = 10V$ $T_{min} < T_{op} < T_{max}$	70	90		dB
SVR Supply voltage rejection	$V_i = 1V$ $f = 100 \text{ Hz}$ $T_{min} < T_{op} < T_{max}$	80	100		dB
CS Channel separation	$f = 10 \text{ KHz}$ $R_g = 1 \text{ K}\Omega$		105		dB

(\*) Both amplifiers.



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Fig. 1 - Open loop frequency and phase response

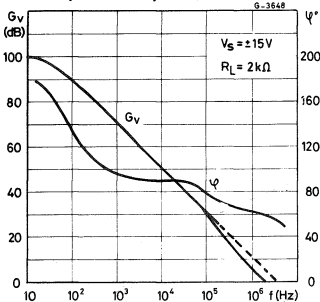


Fig. 2 - Open loop gain vs. ambient temperature

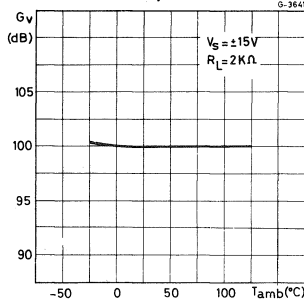


Fig. 3 - Supply voltage rejection vs. frequency

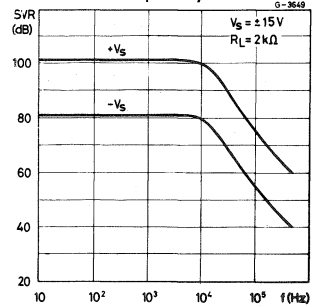


Fig. 4 - Large signal frequency response

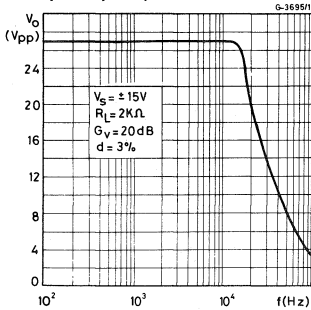


Fig. 5 - Output voltage swing vs. load resistance

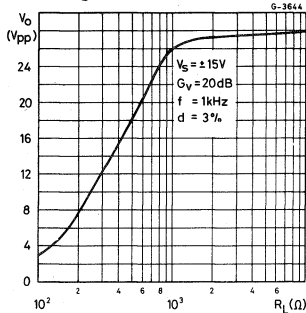


Fig. 6 - Total input noise vs. frequency

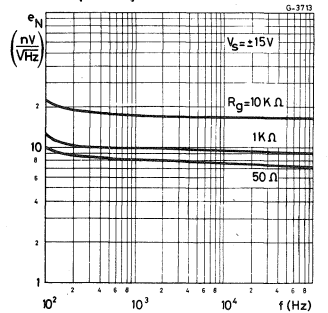


Fig. 7 - Channel separation

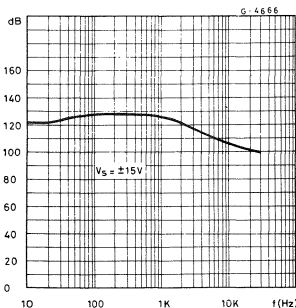


Fig. 8 - Transient response

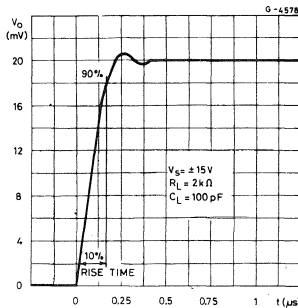
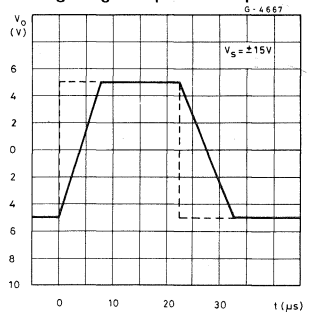
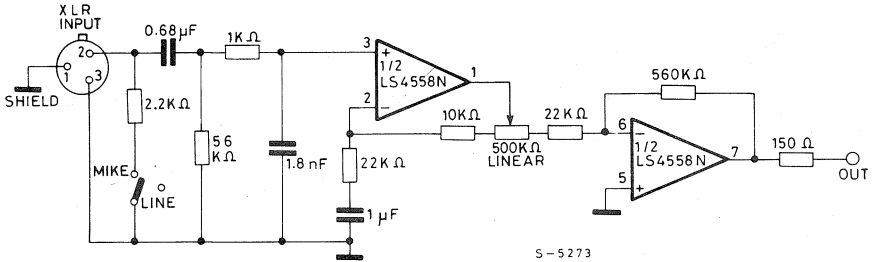


Fig. 9 - Voltage follower large-signal pulse response



## APPLICATION INFORMATION

Fig. 10 - Mike/Line preamplifier for audio mixers (0 dB to 60 dB continuously variable gain)



Note - The particular characteristics of the circuit of fig. 10 is that using a linear potentiometer, the gain is continuously variable in a logarithmic mode from 0 dB to 60 dB in the audio band.

Fig. 11 - Microphones nomograph

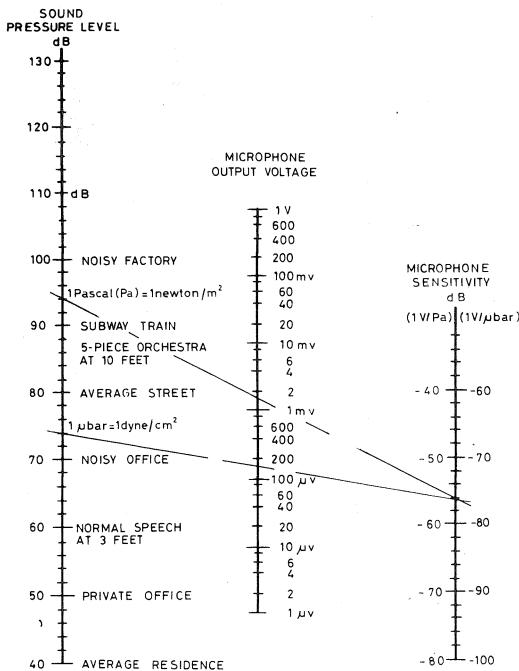


Fig. 12 - Very Low-Noise mike preamplifier ( $G_v = 40$  dB)

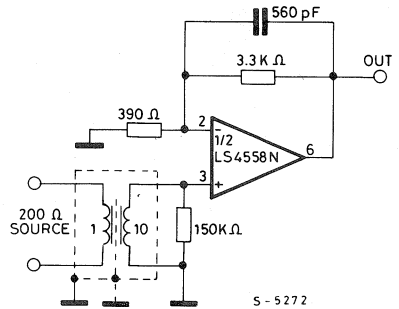
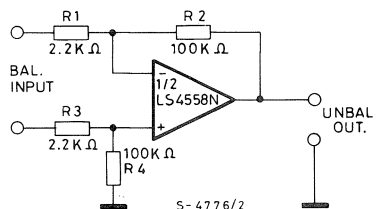


Fig. 13 - Balanced input audio pre-amplifier





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APPLICATION INFORMATION (continued)

Fig. 14 - 20 Hz to 200 Hz variable High-pass filter ( $G_v = 3$  dB)

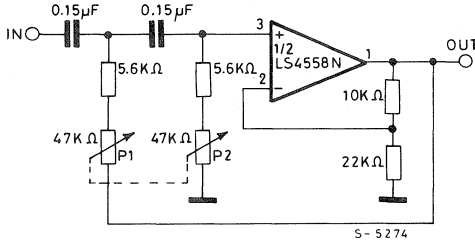


Fig. 15 - Frequency response of the High-pass filter of fig. 14

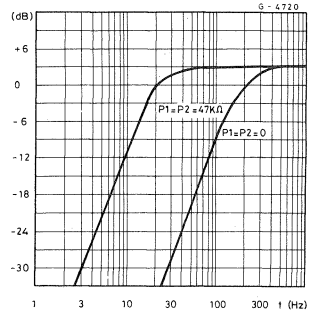


Fig. 16 - DC coupled low-pass active filter ( $f = 1$  KHz,  $G_v = 6$  dB)

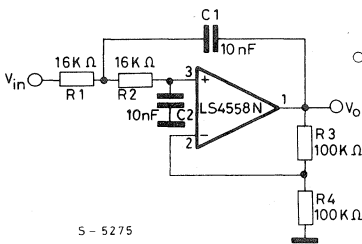


Fig. 17 - Switchable HP-LP audio filter

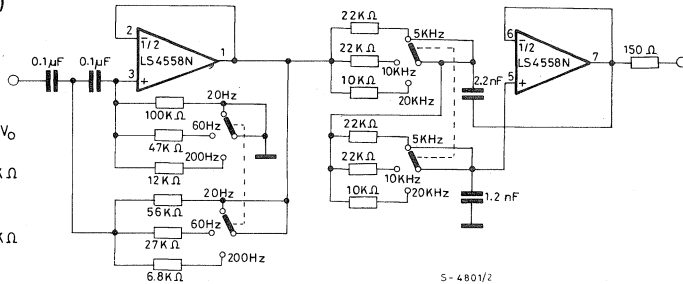
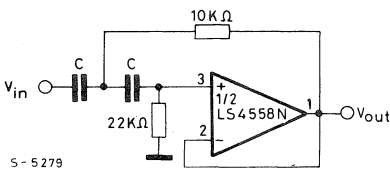
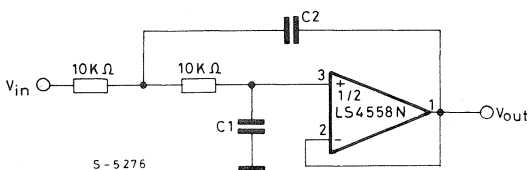


Fig. 18 - Subsonic or rumble filter ( $G_v = 0$  dB)

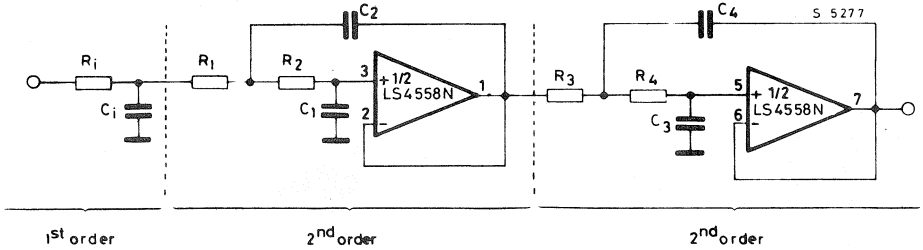


$f_c$ (Hz)	C ( $\mu$ F)
15	0.68
22	0.47
30	0.33
55	0.22
100	0.1

Fig. 19 - High-cut filter ( $G_v = 0$  dB)



$f_c$ (KHz)	C1 (nF)	C2 (nF)
3	3.9	6.8
5	2.2	4.7
10	1.2	2.2
15	0.68	1.5

**APPLICATION INFORMATION (continued)**
**Fig. 20 - Fifth order 3.4 KHz low-pass Butterworth filter**


For  $f_c = 3.4 \text{ KHz}$  and  $R_i = R_1 = R_2 = R_3 = R_4 = 10 \text{ K}\Omega$ , we obtain:

$$C_1 = 1.354 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 6.33 \text{ nF}$$

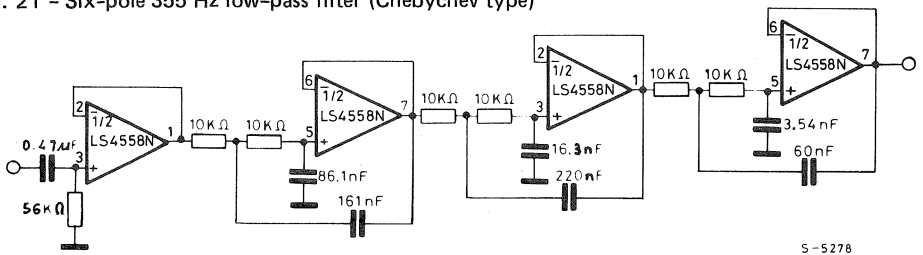
$$C_3 = 0.309 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.45 \text{ nF}$$

$$C_1 = 0.421 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.97 \text{ nF}$$

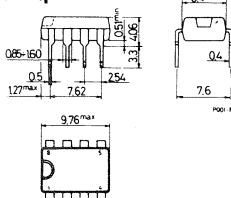
$$C_4 = 3.325 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 15.14 \text{ nF}$$

$$C_2 = 1.753 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 8.20 \text{ nF}$$

The attenuation of the filter is 30 dB at 6.8 KHz and better than 60 dB at 15 KHz.

**Fig. 21 - Six-pole 355 Hz low-pass filter (Chebyshev type)**


This is a 6-pole Chebyshev type with  $\pm 0.25 \text{ dB}$  ripple in the passband. A decoupling stage is used to avoid the influence of the input impedance on the filter's characteristics. The attenuation is about 55 dB at 710 Hz and reaches 80 dB at 1065 Hz. The in band attenuation is limited in practice to the  $\pm 0.25 \text{ dB}$  ripple and does not exceed 0.5 dB at 0.9  $f_c$ .

**MECHANICAL DATA (Dimensions in mm)**
**Minidip**

**SO-8**
